Investigations of Direct Methods for the Determination of Fine Structure Associated with the Velocity Dependence of Total Elastic Scattering Cross-sections for Neutral Particles in the Thermal Energy Range

A Thesis

presented to the Department of Chemistry of Washington and Lee University as the completion of work for Chemistry 272 and partial completion for the Bachelor of Science with Special Attainments in Chemistry degree.

By

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VITA

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INTRODUCTION

The project at hand is an investigation of methods which might be used for the determination of a plot of ln Q vs γr , as shown in Figure 1, where Q is the crosssection, and γr is the relative velocity of interacting particles. Previously, plots of this nature have been obtained only through much diligent and laborious work. At a specifically selected relative velocity, an individual cross-section was measured, via a machine shown schematically in Figure 2. By making measurements at many relative velocities, the desired graph could be constructed.

It is proposed that by making certain modifications (shown in Figure 3) of the instrument, the plot can be displayed on an oscilloscope screen. My work has been concerned with determining the theoretical, practical, and financial feasibility of this proposal. I have been able to show the feasibility, at least on the first two counts.

THEORETICAL

Significance of $-\ln Q$ vs $\ln \gamma r$: The cross-section is the probability of particles in two crossed beams interacting with one another, and it is velocity dependent. If we assume a certain velocity distribution in the source beam, we can measure the effect of different velocities on the cross-section. As the relative velocity of interacting particles increases the collisional cross-section decreases. This effect is a direct result of the interaction time available to the interacting particles.

With reference to Figure 1, as the relative velocity increases (or the ln γr for that matter), the cross-section becomes smaller, and since $0 \leq Q \leq 1$, the ln Q becomes a more negative number. Therefore - ln Q becomes a more positive number. This accounts for the slope of the plot.

As a digression, let us examine Q more closely in order to gain an appreciation for its magnitude. The unit of the cross-section is square centimeters, or area. It is a measure of the area of molecular influence. The radius of this influence is on the order of 10^{-7} cm. Using the equation $A = \pi r^2$, an area on the order of 10^{-14} cm² is obtained.

The minimacin the curve are indicative of the bound or stable states that can exist while the particles are interacting. The distance along the x-axis, between minima is related to the depth of the potential energy well.

As can be seen, the plot yield much information about systems of interacting particles, and it would be desirable to have a fast, convenient, and accurate means of obtaining it.

Basic Mechanics of the Proposed Instrument: Referring to Figure 3, it can be seen that the parts of the instrument include:

1. Oven- for the generation of a source beam of particles,

2. Difining slits- collimation of the beam,

3. Source beam chopper- pulses the source beam,

4. Flight tube- length allows velocity selection among particles within a give pulse,

5. Cross target beam- used to interact with source beam,

6. Target beam chopper- pulses target beam,

7. Vacuum pumps- evacuation of flight tube, oven, and detector chambers to 10^{-6} - 10^{-7} torr,

8. Detector- detects the intensity of the source beam after interaction,

9. Electronics for taking the ln of the output signal of detector,

10. Oscilloscope screen- displays the desired plot.

For a gas which is in termal equilibrium, the Maxwellian distribution law will hold.

If we arrange things so that the diameter or width of the defining slits is less than or equal to the mean free path of the molecules in the oven, the beam be governed by the laws of effusive flow. This is because the number of collisions which occur within the vicinity of the slits is drastically reduced, thereby giving a non-turbulent flow. This is convenient as there is a good mathematical treatment of effusive flow, and because the intensity of the beam is described by a cosine relationship.

Velocity selection and distribution are governed by the length of the tube and period of the pulsing beam. When the source beam particles interact with the target beam they are scattered out of the beam with a resultant attenuation. The detector measures this attenuation and by comparison with the measurements of beam intensity of an unattenuated beam, puts out a signal which can be converted electronically to an ln signal and displayed on the oscilloscope screen.

<u>Reproducing the Conditions which Exist within the Apparatus</u>: As stated previously, the velocity distribution of the particles in the oven is consistent with the Maxwell distribution law,

$$\frac{1}{N} \frac{dn_c}{dc} = 4\pi \left(\frac{m}{2\pi kt}\right) s/2 c^2 e^{-\beta c^2}, (1)$$

Where, N is the total number of molecules in the oven, $(\frac{1}{N})(dn_c/dc)$ is the fraction of molecules in the speed range c to c + dc per unit width

of the interval, m is the mass in grams of one molecule, k is Boltzmann's constant in cgs units, \overline{t} is the absolute temperature in degrees Kelvin, c is the velocity in cgs units, and $\beta = m/2k\overline{t}$. Bigure 4 shows a typical plot of (1/N) (dn_c/dc) vs. c. According to Maxwellian law the most probable velocity, c_{mp} , is $(2kT/m)^{1/2}$, and the root mean square velocity, $(\overline{c^2})^{1/2}$, is $(3kT/m)^{1/2}$, where $(\overline{c^2})^{1/2} > \overline{c} > c_{mp}$.

An expression for the distribution of particles as a function of time spent along the flight tube is now needed (that is an expression for the velocity distribution). According to the laws of effusive flow the number of particles within the velocity range v and v + dv is $c v^3 e^{-\beta v^2} dv$. After time t a particle of velocity v well have undergone a displacement s, where s = vt. Therefore particles in the velocity range v + dv will be spread over a distance ds, where ds = t dv. If I is the number of particles per unit length of the flight tube then,

$$Ids = \partial v^{\mathbf{3}} e^{-\beta v^{\mathbf{2}}} dv , (2)$$

Where, C is a constant of proportionality, v is the velocity and $\beta = m/2kt$. Substituting tdv for ds, one obtains,

Itdv =
$$Cv^3 e^{-\beta v^2} dv$$
.
It = $Cv^3 e^{-\beta v^2}$.
I = $(C/t) v^3 e^{-\beta v^2}$, and since v = s/t ,
I = $C[(s/t)^3/t]e^{-\beta s^2/t^2}$, so that
I = $C(s^3/t^4)e^{-\beta s^2/t^2}$. (3)

Equation (3) is the desired expression. Comparing equation (1) with equation (3), it is seen that the Maxwellian expression has a c^2 term, while equation (3) has a v^3 term (c=v). The reason for this is that the molecules with the greatest probability of escaping into the flight tube are those with the highest velocity. To be sure, some molecules of lower velocity will escape but the probability decreases with decrease in velocity. As a consequence the most probable velocity found in the beam can be shown to be the root mean square velocity, $(\overline{c^2})^{1/2}$, within the oven.

The most probable velocity is that associated with the maximum on the velocity distribution curve. Therefore, equation (3) is used, and the derivative is taken, which is then set equal to zero and solved for v.

$$f(\mathbf{v}) = C\mathbf{v}^3 e^{-\beta \mathbf{v}^2},$$

$$\frac{df(\mathbf{v})}{d\mathbf{v}} = 3C\mathbf{v}^2 e^{-\beta \mathbf{v}^2} - (2\beta \mathbf{v} e^{-\beta \mathbf{v}^2}) C\mathbf{v}^3.$$

Setting this equal to zero, and substituting for β ,

$$0 = \frac{f(v)}{dv} = 3Cv^2 e^{-v^2 m/2kT} - v^3 C(vm/kT) e^{-v^2 m/2kT};$$

$$0 = Cv^2 e^{-v^2 m/2kT} (3 - v^2 m/kT)$$

The condition which determines v_{mp} is ,

$$0 = 3 - v^2 m/kT$$
,
 $v^2 (m/kT) = 3$,
 $v^2 = 3kT/m$
v (effusive flow) = $(3kT/m)^{1/2}$, (4)

Comparison of equation (4) with $(\overline{c}^2)^{1/2}$, for 5 the Maxwellian law shows that,

$$v_{mp}(effusive flow) = (3kT/m)^{1/2} = (\overline{c^2})^{1/2},$$
 (5)

The use of equation (3) in a computer program approximates the condition where there is no cross beam, and where it is taitly assumed that there is no attenuation of the source beam by background gases in the flight tube.

In order to take attenuation by a background gas into account the following equations are used.

$$\frac{\mathbf{I}}{\mathbf{I}} = e^{-\frac{\mathbf{I}}{\lambda}}, \qquad (6)$$

Where, $(I/I^{\circ})_{in}$ the ratio of the attenuated beam to the unattenuated beam, f_{in} the length of the flight tube.

 $\lambda = \pi^{1/2} (v/\alpha)^2 / (n_g Q_{eff} \Psi(v/\alpha)),^1 \quad (7)$

¹Dr. Thomas C. Imeson, Doctoral Thesis.

where, v is the velocity of the molecules in the beam, $\alpha = (2kT/m_g)^{1/2}$ (where m_g is the mass of the attenuating gas), n_g is the number density of the attenuating gas (n_g = [N/Vol.] = [P/kT], units are all cgs), and Q_{eff} is the effective cross-section.

If (v/α) is allowed to equal x, then,

 $\Psi(x) = xe^{-x^2} + (2x^2 + 1) [(2/\pi^{1/2}) \int_{0}^{2} e^{-t^2} dt], \quad (8)$ where the factor $(2/\pi^{1/2}) \int_{0}^{2} e^{-t^2} dt$ is the error function (erf). This integral cannot be evaluated by ordinary integration techniques. In a computer it can be approximated by,

erf= $(2/\pi^{1/2})[1.0-(1.0/\{1.0+A_1\cdot x^2+A_3\cdot x^3+A_4\cdot x^4+A_5\cdot x^5+A_6\cdot x^6\}^{16})]^1$, (9) where, $A_1 = .07052308$, $A_2 = .04228202$,

 $A_3 = .00927057$,

 $A_4 = .00015604$

 $A_5 = .00027257,$

 $A_{6} = .00004303,$

 Q_{eff} in equation (7) can be approximated roughly by the equation 2 ,

$$Q_{eff} = Q_{o} (1/v)^{2/(s-1)},$$
 (10)

where, s = 6.1, v is velocity of beam particles, and $Q_0 = e^{5 \cdot 37} (kT/d)$, where d = 1.27 cm.

The next step which must be taken is the calculation of the absolute intensity as a function of the angle measured from a normal to the slit (or detector). The equation used is,

$$I = (1/n) (dn_v/dv) = 2\pi A(v^3/t) e^{-\beta v^2} \sin \theta \cos \theta d\theta^3, \quad (11)$$

¹Cecil Hastings, Jr., <u>Approximations for Digital Computers</u>, p. 187, (1966), Princeton University Press.

²M. M. Hessel and P. Kusch, "Deviations from the 1/r⁶ potential in Scattering of a Polar Molecule by Non-Polar Gases," <u>J. Chem. Phys.</u> 43, 305, (1965).

³Earle H. Kennard, <u>Kinetic Theory of Gases</u>, pp. 61-64, (1938), McGraw-Hill Book Company, Inc. where, $A = (\rho/\pi)^{3/2}$, θ is the angle measured from the normal to the slit, and $d\theta$ is the radius of the detector. Equation (11) can be rewritten slightly so that,

$$I = 2\pi (m/2kT_{\pi})^{3/2} (s^{3}/t^{4})e^{-mv^{2}/2kT}, \qquad (12)$$

where s is the length of the flight tube. Using equation (12), the absolute intensity can be calculated as a function of θ for a flight tube length of two meters (assuming 10⁶ torr background air pressure, and detector area of 3 \times 10⁴ sq. in.).

EXPERIMENTAL

Experimental Results: The following data are for potassium, cesium, and rubidium at an oven temperature of 4500° K, with flight tube lengths of 50.0 cm, 100.0 cm, 150.0 cm, 200.0 cm, and 250.0 cm. The first three plots are I vs S, with five constant times. The times are calculated using the equation t = s/v, where for each elements $v = v_{mp}$ (effusive flow), and a time is obtained for each flight tube length.

These graphs are fairly insensitive because of the large increment of distant (9.0 cm) along the x-axis. That is, the velocity spread is compressed. Nevertheless, a first approximation of the tube lengths which will yield the best velocity distribution, with the least attenuation of intensity can be made. These lengths are 150.0 cm, 200.0 cm, and 250.0 cm.

In order to narrow down the choices further, the next three plots are used. These are I vs t, and are much more sensitive, because (keeping the above three distances constant) the increment of t is on the order of 10^{-4} sec. This is a much smaller increment along the x-axis, and has the effect of expanding the velocity spread. According to these data a flight tube distance of 150.0 cm to 200.0 cm is appropriate, because the distribution of velocities for the flight tube of 250.0 cm is spread over too great a range with a resultant loss in intensity.

The last set of data is a table of values for the attenuation of a beam of potassium atoms, due to the background scattering of nitrogen in the flight tube. Tube lengths and velocities used are thos obtained from the second set of graphs. (I/I°) , the attenuation, is calculated at a flight tube temperature of 300° K, and pressures of 10^{-5} , 10^{-6} , and 10^{-7} torr. The data show that for both tube lengths, at a pressure of 10^{-7} torr, (I/I°) is very close to 1. That is, attenuation is small. It might well be noted that a tube length of 150.0 cm gives slightly better results.

8.

MAXWEL	LLIAN DISTRIBUT	ION, AND DISTR	IBUTION IN E	FFUSIVE FLOW			0.
TYPE (OF ATOM IS K	MASS= 0.64953	E-22GRAMS	TEMPERATURE=	450.0	DEG. K.	
 ACCORI RMSV= (DING TO MAXWELL. (3KT/M)**.5	IAN DISTRIBUTI	ON, VMP=(2KT	/M)**.5, AV=	(8KT/3	•141M)**•5•	
VMP= (0.43734E 05CM/SI	EC AV= 0.493	53E 05CM/SEC	RMSV= 0.5	3563E	05CM/SEC	
ACCORD	ING TO EFFUSIV	E FLOW DISTRIB	UTION. VMP=(3KT/M)#*.5.			
AV=.75	5(2*3.141KT/M)*	.5, RMSV=(KT/	M) **.5				
VMP≖ (0.53563E 05CM/SI	EC AV= 0.581	32E 05CM/SEC	RMSV= 0.3	0924E	05CM/SEC	
TIME=	0.933E-03SEC	DISTANCE= 0	.500E 02CM	FOR POINTS	1		
TIME=	0.186E-02SEC	DISTANCE= 0	.100E 03CM	FOR POINTS	2		
TIME=	0.280E-02SEC	DISTANCE= 0	.150E 03CM	FOR POINTS	3		
TIME=	0.373E-02SEC	DISTANCE= 0	.200E 03CM	FOR POINTS	4		
TIME=	0.466E-02SEC	DISTANCE= 0	.250E 03CM	FOR POINTS	5		
PLOT O	OF I VS S ACCORC	DING TO THE EQ	UATION I=C(S	**3/T* * 4)*E*	*(-85*	*2/T**2)	
PLOT O INCREM STEP	DF I VS S ACCORC MENT ALONG X-AXI DISTANCE(IN CM)	DING TO THE EQ S= 9.0CM, POINTS 1	UATION I=C(S CONSTANT TIM POINTS 2	**3/T**4)*E* E UNNORMA POINTS	*(85* LIZED 3	*2/T**2) DATA POINTS 4	POINTS
PLOT O INCREM STEP 1	DF I VS S ACCORC MENT ALONG X-AXI DISTANCE(IN CM) 0.0	DING TO THE EQ S= 9.0CM, POINTS 1 0.000E 00	UATION I=C(S CONSTANT TIM POINTS 2 0.000E 00	**3/T**4)*E* E UNNORMA POINTS 0 0.000E	*(85* LIZED 3 00	*2/T**2) DATA POINTS 4 0.000E 00	POINTS 0.000E
PLOT O INCREM STEP 1 2	DF I VS S ACCORC MENT ALONG X-AXI DISTANCE(IN CM) 0.0 9.0	DING TO THE EQ S= 9.0CM, POINTS 1 0.000E 00 0.914E 15	UATION I=C(S CONSTANT TIME POINTS 2 0.000E 00 0.592E 14	**3/T**4)*E* E UNNORMA POINTS 0 0.000E 4 0.117E	*(-8S* LIZED 3 00 14	*2/T**2) DATA POINTS 4 0.000E 00 0.373E 13	POINTS 0.000E 0.153E
PLOT O INCREM STEP 1 2 3	DF I VS S ACCORC MENT ALONG X-AXI DISTANCE(IN CM) 0.0 9.0 18.0	DING TO THE EQ S= 9.0CM, POINTS 1 0.000E 00 0.914E 15 0.632E 16	UATION I=C(S CONSTANT TIM POINTS 2 0.000E 00 0.592E 14 0.457E 15	**3/T**4)*E* E UNNORMA POINTS 0 0.000E 4 0.117E 5 0.928E	*(BS* 3 00 14 14	*2/T**2) DATA POINTS 4 0.000E 00 0.373E 13 0.296E 14	POINTS 0.000E 0.153E 0.121E
PLOT O INCREM STEP 1 2 3 4	DF I VS S ACCORO MENT ALONG X-AXI DISTANCE(IN CM) 0.0 9.0 18.0 27.0	DING TO THE EQ S= 9.0CM, POINTS 1 0.000E 00 0.914E 15 0.632E 16 0.167E 17	UATION I=C(S CONSTANT TIME POINTS 2 0.000E 00 0.592E 14 0.457E 15 0.145E 10	**3/T**4)*E* E UNNORMA POINTS 0 0.000E 4 0.117E 5 0.928E 5 0.304E	*(BS* 3 00 14 14 15	*2/T**2) DATA POINTS 4 0.000E 00 0.373E 13 0.296E 14 0.985E 14	POINTS 0.000E 0.153E 0.121E 0.407E
PLOT O INCREM STEP 1 2 3 4 5	DF I VS S ACCORC MENT ALONG X-AXI DISTANCE(IN CM) 0.0 9.0 18.0 27.0 36.0	DING TO THE EQ S= 9.0CM, POINTS 1 0.000E 00 0.914E 15 0.632E 16 0.167E 17 0.282E 17	UATION I=C(S+ CONSTANT TIME POINTS 2 0.000E 00 0.592E 14 0.457E 15 0.145E 16 0.316E 16	**3/T**4)*E* E UNNORMA POINTS 0 0.000E 4 0.117E 5 0.928E 6 0.304E 6 0.695E	*(8S* 3 00 14 14 15 15	*2/T**2) DATA POINTS 4 0.000E 00 0.373E 13 0.296E 14 0.985E 14 0.228E 15	POINTS 0.000E 0.153E 0.121E 0.407E 0.953E
PLOT O INCREM STEP 1 2 3 4 5 6	DF I VS S ACCORC MENT ALONG X-AXI DISTANCE(IN CM) 0.0 9.0 18.0 27.0 36.0 45.0	DING TO THE EQ S= 9.0CM, POINTS 1 0.000E 00 0.914E 15 0.632E 16 0.167E 17 0.282E 17 0.356E 17	UATION I=C(S+ CONSTANT TIME POINTS 2 0.000E 00 0.592E 14 0.457E 15 0.145E 16 0.316E 16 0.553E 16	**3/T**4)*E* E UNNORMA POINTS 0 0.000E 4 0.117E 5 0.928E 5 0.304E 6 0.695E 6 0.129E	*(8S* 3 00 14 14 15 15 16	*2/T**2) DATA POINTS 4 0.000E 00 0.373E 13 0.296E 14 0.985E 14 0.228E 15 0.434E 15	POINTS 0.000E 0.153E 0.121E 0.407E 0.953E 0.182E
PLOT 0 INCREM STEP 1 2 3 4 5 6 7	DF I VS S ACCOR MENT ALONG X-AXI DISTANCE(IN CM) 0.0 9.0 18.0 27.0 36.0 45.0 54.0	DING TO THE EQ (S= 9.0CM, POINTS 1 0.000E 00 0.914E 15 0.632E 16 0.167E 17 0.282E 17 0.356E 17 0.360E 17	UATION I=C(S CONSTANT TIM POINTS 2 0.000E 00 0.592E 14 0.457E 15 0.145E 16 0.316E 16 0.553E 16 0.836E 16	**3/T**4)*E* E UNNORMA POINTS 0 0.000E 4 0.117E 5 0.928E 5 0.304E 5 0.695E 6 0.129E 6 0.210E	*(BS* 3 00 14 14 15 15 16 16	*2/T**2) DATA POINTS 4 0.000E 00 0.373E 13 0.296E 14 0.985E 14 0.228E 15 0.434E 15 0.726E 15	POINTS 0.000E 0.153E 0.121E 0.407E 0.953E 0.182E 0.309E
PLOT O INCREM STEP 1 2 3 4 5 6 7 6 7	DF I VS S ACCOR(MENT ALONG X-AX) DISTANCE(IN CM) 0.0 9.0 18.0 27.0 36.0 45.0 54.0 63.0 72.0	DING TO THE EQ (S= 9.0CM, POINTS 1 0.000E 00 0.914E 15 0.632E 16 0.167E 17 0.282E 17 0.356E 17 0.360E 17 0.304E 17 0.304E 17	UATION I=C(S CONSTANT TIME POINTS 2 0.000E 00 0.592E 14 0.457E 15 0.145E 16 0.316E 16 0.553E 16 0.836E 16 0.113E 17	**3/T**4)*E* E UNNORMA POINTS 0 0.000E 4 0.117E 5 0.928E 6 0.304E 6 0.695E 6 0.129E 6 0.210E 7 0.312E	*(BS* 3 00 14 14 15 15 16 16 16	*2/T**2) DATA POINTS 4 0.000E 00 0.373E 13 0.296E 14 0.985E 14 0.228E 15 0.434E 15 0.726E 15 0.110E 16	POINTS 0.000E 0.153E 0.121E 0.407E 0.953E 0.182E 0.309E 0.479E
PLOT 0 INCREM STEP 1 2 3 4 5 6 7 8 9	DF I VS S ACCORC MENT ALONG X-AXI DISTANCE(IN CM) 0.0 9.0 18.0 27.0 36.0 45.0 54.0 63.0 72.0 81.0	DING TO THE EQ S= 9.0CM, POINTS 1 0.000E 00 0.914E 15 0.632E 16 0.167E 17 0.282E 17 0.356E 17 0.360E 17 0.304E 17 0.219E 17	UATION I=C(S CONSTANT TIME POINTS 2 0.000E 00 0.592E 14 0.457E 15 0.145E 16 0.316E 16 0.553E 16 0.836E 16 0.113E 17 0.141E 17 0.141E 17	**3/T**4)*E* E UNNORMA POINTS 0 0.000E 4 0.117E 5 0.928E 6 0.304E 6 0.695E 6 0.129E 6 0.129E 7 0.312E 7 0.429E	<pre>#(BS# 3 00 14 14 15 15 16 16 16 16 16</pre>	*2/T**2) DATA POINTS 4 0.000E 00 0.373E 13 0.296E 14 0.985E 14 0.228E 15 0.434E 15 0.434E 15 0.726E 15 0.110E 16 0.158E 16 0.2325 16	POINTS 0.000E 0.153E 0.121E 0.407E 0.953E 0.182E 0.309E 0.479E 0.479E 0.694E
PLOT 0 INCREM STEP 1 2 3 4 5 6 7 8 9 10 11	DF I VS S ACCORC MENT ALONG X-AXI DISTANCE(IN CM) 0.0 9.0 18.0 27.0 36.0 45.0 54.0 63.0 72.0 81.0 90.0	DING TO THE EQ DING TO THE EQ POINTS 1 0.000E 00 0.914E 15 0.632E 16 0.167E 17 0.282E 17 0.356E 17 0.360E 17 0.304E 17 0.219E 17 0.136E 17 0.744E 16	UATION I=C(S CONSTANT TIME POINTS 2 0.000E 00 0.592E 14 0.457E 15 0.145E 16 0.316E 16 0.553E 16 0.836E 16 0.836E 16 0.113E 17 0.163E 17 0.178E 17	**3/T**4)*E* E UNNORMA POINTS 0 0.000E 4 0.117E 5 0.928E 6 0.304E 6 0.695E 6 0.129E 6 0.129E 6 0.210E 7 0.312E 7 0.429E 7 0.557E 7 0.4905	*(BS* 3 00 14 14 15 15 16 16 16 16 16 16	*2/T**2) DATA POINTS 4 0.000E 00 0.373E 13 0.296E 14 0.985E 14 0.985E 14 0.228E 15 0.434E 15 0.434E 15 0.726E 15 0.110E 16 0.158E 16 0.213E 16 0.276E 14	POINTS 0.000E 0.153E 0.121E 0.407E 0.953E 0.182E 0.309E 0.479E 0.694E 0.956E
PLOT 0 INCREM STEP 1 2 3 4 5 6 7 8 9 10 11 12	DF I VS S ACCOR(MENT ALONG X-AX) DISTANCE(IN CM) 0.0 9.0 18.0 27.0 36.0 45.0 54.0 63.0 72.0 81.0 90.0 99.0	DING TO THE EQ (S= 9.0CM, POINTS 1 0.000E 00 0.914E 15 0.632E 16 0.167E 17 0.282E 17 0.356E 17 0.360E 17 0.360E 17 0.304E 17 0.136E 17 0.136E 17 0.744E 16 0.356E 16	UATION I=C(S CONSTANT TIME POINTS 2 0.000E 00 0.592E 14 0.457E 15 0.145E 16 0.316E 16 0.553E 16 0.836E 16 0.113E 17 0.163E 17 0.163E 17 0.183E 17	**3/T**4)*E* E UNNORMA POINTS 0 0.000E 4 0.117E 5 0.928E 6 0.304E 6 0.695E 6 0.129E 6 0.129E 6 0.210E 7 0.312E 7 0.429E 7 0.557E 7 0.690E 7 0.820E	*(BS* 3 00 14 14 15 15 16 16 16 16 16 16 16	*2/T**2) DATA POINTS 4 0.000E 00 0.373E 13 0.296E 14 0.985E 14 0.228E 15 0.434E 15 0.434E 15 0.726E 15 0.110E 16 0.158E 16 0.213E 16 0.276E 16 0.345E 16	POINTS 0.000E 0.153E 0.121E 0.407E 0.953E 0.182E 0.309E 0.479E 0.694E 0.956E 0.126E 0.141E
PLOT 0 INCREM STEP 1 2 3 4 5 6 7 6 7 8 9 10 11 12 13	DF I VS S ACCORC MENT ALONG X-AXI DISTANCE(IN CM) 0.0 9.0 18.0 27.0 36.0 45.0 54.0 63.0 72.0 81.0 90.0 99.0 108.0	DING TO THE EQ (S= 9.0CM, POINTS 1 0.000E 00 0.914E 15 0.632E 16 0.167E 17 0.282E 17 0.356E 17 0.360E 17 0.304E 17 0.304E 17 0.136E 17 0.744E 16 0.356E 16 0.151E 16	UATION I=C(S) CONSTANT TIME POINTS 2 0.000E 00 0.592E 14 0.457E 19 0.145E 16 0.316E 16 0.553E 16 0.836E 16 0.113E 17 0.141E 17 0.163E 17 0.183E 17 0.180E 17	**3/T**4)*E* E UNNORMA POINTS 0 0.000E 4 0.117E 5 0.928E 6 0.304E 6 0.695E 6 0.129E 6 0.129E 7 0.312E 7 0.312E 7 0.312E 7 0.557E 7 0.690E 7 0.820E 7 0.820E	*(-BS* JZED 3 00 14 14 15 15 16 16 16 16 16 16 16 16 16 16	*2/T**2) DATA POINTS 4 0.000E 00 0.373E 13 0.296E 14 0.985E 14 0.228E 15 0.434E 15 0.434E 15 0.726E 15 0.110E 16 0.158E 16 0.213E 16 0.276E 16 0.345E 16 0.418E 16	POINTS 0.000E 0.153E 0.121E 0.407E 0.953E 0.182E 0.309E 0.479E 0.694E 0.956E 0.126E 0.161E 0.200E
PLOT 0 INCREM STEP 1 2 3 4 5 6 7 8 9 10 11 11 12 13 14	DF I VS S ACCORC MENT ALONG X-AXI DISTANCE(IN CM) 0.0 9.0 18.0 27.0 36.0 45.0 54.0 63.0 72.0 81.0 90.0 99.0 108.0 117.0	DING TO THE EQ (S= 9.0CM, POINTS 1 0.000E 00 0.914E 15 0.632E 16 0.167E 17 0.282E 17 0.356E 17 0.360E 17 0.304E 17 0.304E 17 0.136E 17 0.136E 17 0.744E 16 0.356E 16 0.151E 16 0.571E 15	UATION I=C(S CONSTANT TIM POINTS 2 0.000E 00 0.592E 14 0.457E 19 0.145E 16 0.316E 16 0.316E 16 0.553E 16 0.836E 16 0.113E 17 0.141E 17 0.163E 17 0.183E 17 0.183E 17 0.180E 17 0.169E 17	**3/T**4)*E* E UNNORMA POINTS 0 0.000E 4 0.117E 5 0.928E 5 0.304E 6 0.695E 6 0.129E 6 0.129E 7 0.429E 7 0.312E 7 0.429E 7 0.557E 7 0.690E 7 0.820E 7 0.941E 7 0.104E	<pre># (-8S# J CO 14 14 15 15 16 16 16 16 16 16 16 16 16 16 16 16 16</pre>	*2/T**2) DATA POINTS 4 0.000E 00 0.373E 13 0.296E 14 0.985E 14 0.228E 15 0.434E 15 0.434E 15 0.726E 15 0.110E 16 0.158E 16 0.276E 16 0.345E 16 0.493E 16 0.493E 16	POINTS 0.000E 0.153E 0.121E 0.407E 0.953E 0.182E 0.309E 0.479E 0.694E 0.956E 0.126E 0.161E 0.200E 0.242E
PLOT 0 INCREM STEP 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	DF I VS S ACCORC MENT ALONG X-AXI DISTANCE(IN CM) 0.0 9.0 18.0 27.0 36.0 45.0 54.0 63.0 72.0 81.0 90.0 99.0 108.0 117.0 126.0	DING TO THE EQ S= 9.0CM, POINTS 1 0.000E 00 0.914E 15 0.632E 16 0.167E 17 0.282E 17 0.356E 17 0.360E 17 0.304E 17 0.304E 17 0.136E 17 0.136E 17 0.136E 16 0.356E 16 0.151E 16 0.571E 15 0.192E 15	UATION I=C(S) CONSTANT TIMP POINTS 2 0.000E 00 0.592E 14 0.457E 19 0.145E 16 0.316E 16 0.316E 16 0.553E 16 0.836E 16 0.113E 17 0.163E 17 0.183E 17 0.183E 17 0.189E 17 0.169E 17 0.152E 17	**3/T**4)*E* E UNNORMA POINTS 0 0.000E 4 0.117E 5 0.928E 6 0.304E 6 0.695E 6 0.129E 6 0.129E 7 0.312E 7 0.312E 7 0.312E 7 0.557E 7 0.690E 7 0.820E 7 0.941E 7 0.104E 7 0.112E	<pre># (BS# JOO 14 14 14 15 15 16 16 16 16 16 16 16 16 16 16 16 16 17 17</pre>	*2/T**2) DATA POINTS 4 0.000E 00 0.373E 13 0.296E 14 0.985E 14 0.228E 15 0.434E 15 0.434E 15 0.726E 15 0.110E 16 0.213E 16 0.276E 16 0.345E 16 0.493E 16 0.493E 16 0.567E 16	POINTS 0.000E 0.153E 0.121E 0.407E 0.953E 0.182E 0.309E 0.479E 0.694E 0.956E 0.126E 0.161E 0.200E 0.242E 0.287E
PLOT 0 INCREM STEP 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	DF I VS S ACCORC MENT ALONG X-AXI DISTANCE (IN CM) 0.0 9.0 18.0 27.0 36.0 45.0 54.0 63.0 72.0 81.0 99.0 108.0 117.0 126.0 135.0	DING TO THE EQ (S= 9.0CM, POINTS 1 0.000E 00 0.914E 15 0.632E 16 0.167E 17 0.282E 17 0.356E 17 0.356E 17 0.360E 17 0.304E 17 0.304E 17 0.136E 17 0.136E 17 0.136E 16 0.356E 16 0.571E 15 0.192E 15 0.577E 14	UATION I=C(S CONSTANT TIME POINTS 2 0.000E 00 0.592E 14 0.457E 15 0.145E 16 0.316E 16 0.553E 16 0.836E 16 0.113E 17 0.163E 17 0.183E 17 0.183E 17 0.180E 17 0.169E 17 0.152E 17 0.131E 17	**3/T**4)*E* EUNNORMA POINTS 0 0.000E 4 0.117E 5 0.928E 6 0.304E 6 0.695E 6 0.129E 6 0.129E 7 0.312E 7 0.312E 7 0.429E 7 0.557E 7 0.690E 7 0.820E 7 0.941E 7 0.104E 7 0.118E	<pre>#(-BS# 3 00 14 14 15 15 16 16 16 16 16 16 16 16 16 16 16 16 16</pre>	*2/T**2) DATA POINTS 4 0.000E 00 0.373E 13 0.296E 14 0.985E 14 0.228E 15 0.434E 15 0.434E 15 0.726E 15 0.110E 16 0.213E 16 0.213E 16 0.276E 16 0.345E 16 0.493E 16 0.493E 16 0.567E 16 0.639E 16	POINTS 0.000E 0.153E 0.121E 0.407E 0.953E 0.182E 0.309E 0.479E 0.694E 0.956E 0.126E 0.126E 0.126E 0.126E 0.200E 0.242E 0.287E 0.334E
PLOT 0 INCREM STEP 1 2 3 4 5 6 7 6 7 6 7 8 9 10 11 12 13 14 15 16 17	DF I VS S ACCORC MENT ALONG X-AXI DISTANCE(IN CM) 0.0 9.0 18.0 27.0 36.0 45.0 54.0 63.0 72.0 81.0 90.0 99.0 108.0 117.0 126.0 135.0 144.0	DING TO THE EQ (S= 9.0CM, POINTS 1 0.000E 00 0.914E 15 0.632E 16 0.167E 17 0.282E 17 0.356E 17 0.356E 17 0.360E 17 0.360E 17 0.360E 17 0.360E 17 0.360E 17 0.366E 16 0.571E 15 0.192E 15 0.577E 14 0.155E 14	UATION I=C(S) CONSTANT TIME POINTS 2 0.000E 00 0.592E 14 0.457E 19 0.145E 16 0.316E 16 0.316E 16 0.553E 16 0.131E 17 0.169E 17 0.16	**3/T**4)*E* E UNNORMA POINTS 0 0.000E 4 0.117E 5 0.928E 6 0.304E 6 0.695E 6 0.129E 6 0.129E 7 0.429E 7 0.429E 7 0.557E 7 0.690E 7 0.820E 7 0.820E 7 0.104E 7 0.112E 7 0.121E	*(BS* 3 00 14 14 15 15 16 16 16 16 16 16 16 16 16 16 16 16 16	*2/T**2) DATA POINTS 4 0.000E 00 0.373E 13 0.296E 14 0.985E 14 0.985E 14 0.228E 15 0.434E 15 0.434E 15 0.726E 15 0.110E 16 0.213E 16 0.213E 16 0.345E 16 0.418E 16 0.493E 16 0.567E 16 0.639E 16 0.705E 16	POINTS 0.000E 0.153E 0.121E 0.407E 0.953E 0.182E 0.309E 0.479E 0.694E 0.694E 0.956E 0.126E 0.161E 0.200E 0.242E 0.287E 0.334E 0.382E
PLOT 0 INCREM STEP 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	DF I VS S ACCORC MENT ALONG X-AXI DISTANCE(IN CM) 0.0 9.0 18.0 27.0 36.0 45.0 54.0 63.0 72.0 81.0 90.0 99.0 108.0 117.0 126.0 135.0 144.0	DING TO THE EQ (S= 9.0CM, POINTS 1 0.000E 00 0.914E 15 0.632E 16 0.167E 17 0.282E 17 0.356E 17 0.360E 17 0.360E 17 0.304E 17 0.304E 17 0.136E 17 0.136E 17 0.136E 17 0.136E 16 0.571E 15 0.192E 15 0.577E 14 0.374E 13	UATION 1=C(S) CONSTANT TIME POINTS 2 0.000E 00 0.592E 14 0.457E 19 0.145E 16 0.316E 16 0.316E 16 0.553E 16 0.836E 16 0.141E 17 0.163E 17 0.163E 17 0.180E 17 0.169E 17 0.152E 17 0.131E 17 0.109E 17 0.880E 16	**3/T**4)*E* E UNNORMA POINTS 0 0.000E 4 0.117E 5 0.928E 6 0.304E 6 0.695E 6 0.129E 6 0.129E 7 0.312E 7 0.312E 7 0.557E 7 0.690E 7 0.820E 7 0.941E 7 0.104E 7 0.118E 7 0.121E 5 0.122E	*(-BS* LIZED 3 00 14 14 15 15 16 16 16 16 16 16 16 16 16 16	*2/T**2) DATA POINTS 4 0.000E 00 0.373E 13 0.296E 14 0.985E 14 0.985E 14 0.228E 15 0.434E 15 0.434E 15 0.726E 15 0.110E 16 0.213E 16 0.213E 16 0.213E 16 0.493E 16 0.493E 16 0.493E 16 0.639E 16 0.705E 16 0.765E 16	POINTS 0.000E 0.153E 0.121E 0.407E 0.953E 0.182E 0.309E 0.479E 0.694E 0.956E 0.126E 0.126E 0.126E 0.126E 0.200E 0.242E 0.287E 0.334E 0.382E 0.430E
PLOT 0 INCREM STEP 1 2 3 4 5 6 7 8 9 10 11 12 13 10 11 12 13 14 15 16 17 18 19	DF I VS S ACCORC MENT ALONG X-AXI DISTANCE(IN CM) 0.0 9.0 18.0 27.0 36.0 45.0 54.0 63.0 72.0 81.0 90.0 99.0 108.0 117.0 126.0 135.0 144.0 153.0 162.0	DING TO THE EQ (S= 9.0CM, POINTS 1 0.000E 00 0.914E 15 0.632E 16 0.167E 17 0.282E 17 0.356E 17 0.360E 17 0.304E 17 0.304E 17 0.304E 17 0.136E 17 0.136E 17 0.136E 16 0.571E 15 0.192E 15 0.577E 14 0.374E 13 0.812E 12	UATION I=C(S) CONSTANT TIME POINTS 2 0.000E 00 0.592E 14 0.457E 19 0.145E 16 0.316E 16 0.316E 16 0.553E 16 0.836E 16 0.13E 17 0.163E 17 0.163E 17 0.163E 17 0.180E 17 0.169E 17 0.169E 17 0.152E 17 0.131E 17 0.109E 17 0.880E 16 0.682E 16	**3/T**4)*E* E UNNORMA POINTS 0 0.000E 4 0.117E 5 0.928E 6 0.304E 6 0.695E 6 0.129E 7 0.429E 7 0.429E 7 0.557E 7 0.690E 7 0.820E 7 0.820E 7 0.941E 7 0.104E 7 0.104E 7 0.12E 7 0.12E 7 0.12E 5 0.120E	<pre>#(-8S# JZED 3 00 14 14 15 15 16 16 16 16 16 16 16 16 16 16 16 16 17 17 17 17 17 17 17 17</pre>	*2/T**2) DATA POINTS 4 0.000E 00 0.373E 13 0.296E 14 0.985E 14 0.228E 15 0.434E 15 0.434E 15 0.726E 15 0.110E 16 0.158E 16 0.213E 16 0.276E 16 0.493E 16 0.493E 16 0.493E 16 0.493E 16 0.639E 16 0.705E 16 0.765E 16 0.817E 16	POINTS 0.000E 0.153E 0.121E 0.407E 0.953E 0.182E 0.309E 0.479E 0.694E 0.956E 0.126E 0.126E 0.126E 0.242E 0.287E 0.334E 0.382E 0.430E 0.477E
PLOT 0 INCREM STEP 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	DF I VS S ACCORC MENT ALONG X-AXI DISTANCE(IN CM) 0.0 9.0 18.0 27.0 36.0 45.0 54.0 63.0 72.0 81.0 90.0 99.0 108.0 117.0 126.0 135.0 144.0 153.0 162.0 171.0	DING TO THE EQ (S= 9.0CM, POINTS 1 0.000E 00 0.914E 15 0.632E 16 0.167E 17 0.282E 17 0.356E 17 0.360E 17 0.360E 17 0.304E 17 0.304E 17 0.136E 17 0.136E 17 0.136E 17 0.571E 16 0.571E 15 0.577E 14 0.374E 13 0.812E 12 0.158E 12	UATION I=C(S CONSTANT TIME POINTS 2 0.000E 00 0.592E 14 0.457E 19 0.145E 16 0.316E 16 0.316E 16 0.553E 16 0.836E 16 0.131E 17 0.163E 17 0.163E 17 0.183E 17 0.185E 17 0.185	**3/T**4)*E* E UNNORMA POINTS 0 0.000E 4 0.117E 5 0.928E 6 0.304E 6 0.695E 6 0.129E 7 0.312E 7 0.312E 7 0.312E 7 0.312E 7 0.557E 7 0.690E 7 0.820E 7 0.941E 7 0.104E 7 0.104E 7 0.12E 7 0.12E 7 0.12E 6 0.120E 6 0.120E	<pre>#(BS# JOO 14 14 15 15 16 16 16 16 16 16 16 16 16 16 16 17 17 17 17 17 17 17 17 17</pre>	*2/T**2) DATA POINTS 4 0.000E 00 0.373E 13 0.296E 14 0.985E 14 0.228E 15 0.434E 15 0.434E 15 0.726E 15 0.110E 16 0.213E 16 0.276E 16 0.345E 16 0.493E 16 0.493E 16 0.493E 16 0.567E 16 0.765E 16 0.765E 16 0.817E 16 0.859E 16	POINTS 0.000E 0.153E 0.121E 0.407E 0.953E 0.182E 0.309E 0.479E 0.479E 0.694E 0.956E 0.126E 0.126E 0.126E 0.200E 0.242E 0.287E 0.334E 0.382E 0.430E 0.430E 0.477E 0.522E
PLOT 0 INCREM STEP 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	DF I VS S ACCORC MENT ALONG X-AXI DISTANCE (IN CM) 0.0 9.0 18.0 27.0 36.0 45.0 54.0 63.0 72.0 81.0 90.0 99.0 108.0 117.0 126.0 135.0 144.0 153.0 162.0 171.0 180.0	DING TO THE EQ (S= 9.0CM, POINTS 1 0.000E 00 0.914E 15 0.632E 16 0.167E 17 0.282E 17 0.356E 17 0.360E 17 0.360E 17 0.360E 17 0.360E 17 0.360E 17 0.360E 17 0.360E 17 0.360E 17 0.360E 17 0.356E 16 0.571E 15 0.151E 16 0.577E 14 0.374E 13 0.812E 12 0.158E 12 0.277E 11	UATION I=C(S) CONSTANT TIME POINTS 2 0.000E 00 0.592E 14 0.457E 15 0.145E 16 0.316E 16 0.316E 16 0.553E 16 0.131E 17 0.163E 17 0.163E 17 0.163E 17 0.163E 17 0.169E 16 0.169E 16 0.16	**3/T**4)*E* E UNNORMA POINTS 0 0.000E 4 0.117E 5 0.928E 6 0.304E 6 0.695E 6 0.129E 6 0.129E 7 0.312E 7 0.429E 7 0.557E 7 0.690E 7 0.557E 7 0.690E 7 0.820E 7 0.941E 7 0.104E 7 0.118E 7 0.12E 5 0.125 6 0.129E 6 0.129E 7 0.125 7 0.155 7 0.1557 7 0.1557 7 0.1557 7 0.1557 7 0.1557 7 0.1557 7 0.1557 7 0.15577 7 0.155777 7 0.155777777777777777777	*(-BS* LIZED 3 00 14 14 15 15 16 16 16 16 16 16 16 16 16 16	*2/T**2) DATA POINTS 4 0.000E 00 0.373E 13 0.296E 14 0.985E 14 0.985E 14 0.228E 15 0.434E 15 0.726E 15 0.110E 16 0.158E 16 0.213E 16 0.213E 16 0.276E 16 0.493E 16 0.493E 16 0.493E 16 0.639E 16 0.765E 16 0.859E 16 0.859E 16 0.890E 16	POINTS 0.000E 0.153E 0.121E 0.407E 0.953E 0.182E 0.309E 0.479E 0.694E 0.956E 0.126E 0.161E 0.200E 0.242E 0.287E 0.334E 0.382E 0.382E 0.382E 0.430E 0.430E 0.477E 0.522E 0.564E
PLOT 0 INCREM STEP 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	DF I VS S ACCORC MENT ALONG X-AXI DISTANCE (IN CM) 0.0 9.0 18.0 27.0 36.0 45.0 54.0 63.0 72.0 81.0 90.0 99.0 108.0 117.0 126.0 135.0 144.0 153.0 162.0 171.0 180.0 189.0	DING TO THE EQ (S= 9.0CM, POINTS 1 0.000E 00 0.914E 15 0.632E 16 0.167E 17 0.282E 17 0.356E 17 0.360E 17 0.360E 17 0.360E 17 0.304E 17 0.304E 17 0.304E 17 0.304E 17 0.356E 16 0.571E 15 0.151E 16 0.577E 14 0.577E 12 0.577E 11 0.437E 10	UATION I=C(S) CONSTANT TIME POINTS 2 0.000E 00 0.592E 14 0.457E 19 0.145E 16 0.316E 16 0.553E 16 0.836E 16 0.131E 17 0.163E 17 0.163E 17 0.163E 17 0.163E 17 0.169E 17 0.16	**3/T**4)*E* E UNNORMA POINTS 0 0.000E 4 0.117E 5 0.928E 6 0.304E 6 0.695E 6 0.129E 6 0.210E 7 0.312E 7 0.429E 7 0.557E 7 0.690E 7 0.820E 7 0.820E 7 0.820E 7 0.104E 7 0.118E 7 0.12E 5 0.122E 5 0.120E 5 0.109E 5 0.109E	<pre>#(-BS# IZED 3 00 14 14 15 15 16 16 16 16 16 16 16 16 16 16 16 16 16</pre>	*2/T**2) DATA POINTS 4 0.000E 00 0.373E 13 0.296E 14 0.985E 14 0.985E 14 0.228E 15 0.434E 15 0.434E 15 0.726E 15 0.110E 16 0.158E 16 0.213E 16 0.213E 16 0.493E 16 0.493E 16 0.493E 16 0.639E 16 0.859E 16 0.890E 16 0.909E 16	POINTS 0.000E 0.153E 0.121E 0.407E 0.953E 0.182E 0.309E 0.479E 0.694E 0.956E 0.126E 0.126E 0.126E 0.126E 0.126E 0.242E 0.287E 0.287E 0.334E 0.382E 0.334E 0.382E 0.430E 0.477E 0.522E 0.564E 0.603E
PLOT 0 INCREM STEP 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	DF I VS S ACCORC MENT ALONG X-AXI DISTANCE(IN CM) 0.0 9.0 18.0 27.0 36.0 45.0 54.0 63.0 72.0 81.0 90.0 99.0 108.0 117.0 126.0 135.0 144.0 153.0 162.0 171.0 180.0 198.0	DING TO THE EQ (S= 9.0CM, POINTS 1 0.000E 00 0.914E 15 0.632E 16 0.167E 17 0.282E 17 0.356E 17 0.360E 17 0.360E 17 0.304E 17 0.304E 17 0.304E 17 0.304E 17 0.304E 17 0.356E 16 0.356E 16 0.571E 15 0.151E 16 0.577E 14 0.374E 13 0.812E 12 0.277E 11 0.437E 10 0.622E 09	UATION I=C(S) CONSTANT TIME POINTS 2 0.000E 00 0.592E 14 0.457E 19 0.145E 16 0.316E 16 0.553E 16 0.836E 16 0.13E 17 0.163E 17 0.163E 17 0.163E 17 0.169E 17 0.169E 17 0.169E 17 0.131E 17 0.169E 17 0.131E 17 0.169E 17 0.131E 17 0.169E 16 0.178E 16 0.261E 16 0.178E 16	**3/T**4)*E* E UNNORMA POINTS 0 0.000E 4 0.117E 5 0.928E 5 0.304E 5 0.695E 6 0.129E 6 0.129E 7 0.312E 7 0.312E 7 0.312E 7 0.557E 7 0.690E 7 0.557E 7 0.690E 7 0.820E 7 0.941E 7 0.104E 7 0.12E 7 0.12E 7 0.12E 5 0.12E 5 0.12E 5 0.109E 5 0.109E	*(-BS* LIZED 3 00 14 14 15 15 16 16 16 16 16 16 16 16 16 16	*2/T**2) DATA POINTS 4 0.000E 00 0.373E 13 0.296E 14 0.985E 14 0.228E 15 0.434E 15 0.434E 15 0.726E 15 0.110E 16 0.158E 16 0.213E 16 0.213E 16 0.493E 16 0.493E 16 0.639E 16 0.859E 16 0.890E 16 0.909E 16 0.918E 16	POINTS 0.000E 0.153E 0.121E 0.407E 0.953E 0.182E 0.309E 0.479E 0.694E 0.956E 0.126E 0.126E 0.200E 0.242E 0.287E 0.334E 0.382E 0.334E 0.382E 0.430E 0.477E 0.522E 0.564E 0.603E 0.638E
PLOT 0 INCREM STEP 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	DF I VS S ACCORC MENT ALONG X-AXI DISTANCE(IN CM) 0.0 9.0 18.0 27.0 36.0 45.0 54.0 63.0 72.0 81.0 90.0 99.0 108.0 108.0 117.0 126.0 135.0 144.0 153.0 162.0 171.0 189.0 198.0 207.0	DING TO THE EQ (S= 9.0CM, POINTS 1 0.000E 00 0.914E 15 0.632E 16 0.167E 17 0.282E 17 0.356E 17 0.360E 17 0.360E 17 0.304E 17 0.304E 17 0.304E 17 0.304E 17 0.304E 17 0.304E 17 0.356E 16 0.356E 16 0.571E 15 0.192E 15 0.577E 14 0.374E 13 0.812E 12 0.277E 11 0.437E 10 0.622E 09 0.798E 08	UATION I=C(S) CONSTANT TIME POINTS 2 0.000E 00 0.592E 14 0.457E 19 0.145E 16 0.316E 16 0.316E 16 0.553E 16 0.836E 16 0.13E 17 0.163E 17 0.163E 17 0.163E 17 0.169E 16 0.372E 16 0.178E 16 0.118E 16	**3/T**4)*E* E UNNORMA POINTS 0 0.000E 4 0.117E 5 0.928E 6 0.304E 6 0.695E 6 0.129E 7 0.312E 7 0.312E 7 0.312E 7 0.557E 7 0.690E 7 0.557E 7 0.690E 7 0.820E 7 0.104E 7 0.104E 7 0.121E 5 0.122E 5 0.122E 5 0.125 6 0.128E 7 0.1018E 7 0.1018E 7 0.1018E 7 0.1018E 7 0.1018E 7 0.1018E 7 0.1018E 7 0.1018E 7 0.1018E 7 0.1018E 5 0.109E 5 0.1018E 5 0.1018E 5 0.1018E 5 0.1018E 5 0.828E	<pre>#(-8S# LIZED 3 00 14 14 15 15 16 16 16 16 16 16 16 16 16 16 16 17 17 17 17 17 17 17 17 17 17 17 17 17</pre>	*2/T**2) DATA POINTS 4 0.000E 00 0.373E 13 0.296E 14 0.985E 14 0.228E 15 0.434E 15 0.434E 15 0.726E 15 0.110E 16 0.158E 16 0.213E 16 0.276E 16 0.493E 16 0.493E 16 0.493E 16 0.765E 16 0.859E 16 0.890E 16 0.918E 16 0.915E 16	POINTS 0.000E 0.153E 0.121E 0.407E 0.953E 0.182E 0.309E 0.479E 0.694E 0.956E 0.126E 0.126E 0.126E 0.242E 0.287E 0.287E 0.334E 0.382E 0.334E 0.382E 0.430E 0.477E 0.522E 0.564E 0.603E 0.638E 0.668E
PLOT 0 INCREM STEP 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25	DF I VS S ACCORC MENT ALONG X-AXI DISTANCE(IN CM) 0.0 9.0 18.0 27.0 36.0 45.0 54.0 63.0 72.0 81.0 90.0 99.0 108.0 108.0 117.0 126.0 135.0 144.0 153.0 162.0 171.0 180.0 189.0 198.0 207.0 216.0	DING TO THE EQ (S= 9.0CM, POINTS 1 0.000E 00 0.914E 15 0.632E 16 0.167E 17 0.282E 17 0.356E 17 0.360E 17 0.360E 17 0.304E 17 0.304E 17 0.304E 17 0.304E 17 0.304E 17 0.356E 16 0.356E 16 0.356E 16 0.571E 15 0.577E 14 0.374E 13 0.812E 12 0.158E 12 0.277E 11 0.437E 10 0.622E 09 0.798E 08 0.923E 07	UATION I=C(S) CONSTANT TIME POINTS 2 0.000E 00 0.592E 14 0.457E 19 0.145E 16 0.316E 16 0.316E 16 0.553E 16 0.836E 16 0.131E 17 0.163E 17 0.163E 17 0.163E 17 0.169E 17 0.169E 17 0.169E 17 0.169E 17 0.169E 17 0.169E 17 0.169E 17 0.169E 16 0.512E 16 0.261E 16 0.178E 16 0.18E 16 0.18E 16 0.757E 15	**3/T**4)*E* UNNORMA POINTS 0 0.000E 4 0.117E 5 0.928E 6 0.304E 6 0.695E 6 0.129E 7 0.312E 7 0.312E 7 0.312E 7 0.312E 7 0.312E 7 0.312E 7 0.429E 7 0.557E 7 0.690E 7 0.820E 7 0.104E 7 0.112E 7 0.112E 7 0.121E 5 0.122E 5 0.122E 5 0.129E 5 0.123E 5 0.129E 5 0.129E	<pre>#(-8S# LIZED 3 00 14 14 15 15 16 16 16 16 16 16 16 16 16 16 17 17 17 17 17 17 17 17 17 17 17 17 17</pre>	*2/T**2) DATA POINTS 4 0.000E 00 0.373E 13 0.296E 14 0.985E 14 0.228E 15 0.434E 15 0.434E 15 0.726E 15 0.110E 16 0.213E 16 0.276E 16 0.276E 16 0.493E 16 0.493E 16 0.493E 16 0.567E 16 0.765E 16 0.859E 16 0.859E 16 0.909E 16 0.915E 16 0.901E 16	POINTS 0.000E 0.153E 0.121E 0.407E 0.953E 0.182E 0.309E 0.479E 0.694E 0.956E 0.126E 0.126E 0.126E 0.287E 0.287E 0.334E 0.382E 0.334E 0.382E 0.430E 0.477E 0.522E 0.564E 0.603E 0.638E 0.668E 0.693E

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	27	234.0	0.910E 05	0.285E 15	0.541E 16	0.845E 16	0.725E 16	
	28	243.0	0.775E 04	0.168E 15	0.455E 16	0.8068 16	0.7326 16	
	29	252.0	0.5978 03	0.9616 14	0.3/75 16	0.760E 16	0.7345 16	
C	31	270 0	0.4150 02	0.0000 14	0.3085 16	0.7108 16	0.730E 16	
	32	279.0	0.1485.00	0.1516 14	0.1965 16	0.6026 16	0.7045 16	
	33	288.0	0.7665-02	0.7766 13	0.1545 16	0.5475 16	0.6875 16	
C	34	297.0	0-356E-03	0.386E 13	0.1186 16	0.493F 16	0.6645 16	
	35	306.0	0.150E-04	0.187E 13	0.906E 15	0.440E 16	0.638E 16	
	36	315.0	0.573E-06	0.884E 12	0.681E 15	0.389E 16	0.608E 16	
(C	37	324.0	0.1986-07	0.406E 12	0.505E 15	0.341E 16	0.577E 16	
	38	333.0	0.619E-09	0.181E 12	0.369E 15	0.296E 16	0.543E 16	
	39	342.0	0.175E-10	0.790E 11	0.267E 15	0.256E 16	0.508E 16	
	40	351.0	0.448E-12	0.335E 11	0.190E 15	0.219E 16	0.473E 16	
	41	360.0	0.104E-13	0.138E 11	0.134E 15	0.186E 16	0.438E 16	
	42	369.0	0.218E-15	0.557E 10	0.933E 14	0.156E 16	0.403E 16	
	43	378.0	0.416E-17	0.218E 10	0.640E 14	0.130E 16	0.368E 16	
	44	387.0	0.0000 00	0.8358 09	0.434E 14	0.1088 16	0.335E 16	
	40	390.U	0.0002 00	0.3112 09	0.2916 14	0.8925 15	0.303E 16	
	47	405.0	0.0005 00	0.1120 09	0.1926 14	0.7286 15	0.2445 14	
	48	423.0	0.000E 00	0.1375 08	0.8126 13	0.4745 15	0.2175 16	
	49	432.0	0.0005 00	0.4615 07	0.5176 13	0.3785 15	0.1925 16	
	50	441.0	0.000E 00	0.1516 07	0.326E 13	0.300F 15	0.1695 16	
	51	450.0	0.0006 00	0.482E 06	0.203E 13	0.2365 15	0.148E 16	
	52	459.0	0.000E 00	0.150E 06	0.124E 13	0.184E 15	0.1298 16	
	53	468.0	0.000E 00	0.455E 05	0.759E 12	0.142E 15	0.112E 16	
	54	477.0	0.000E 00	0.134E 05	0.456E 12	0.109E 15	0.972E 15	
(55	486.0	0.000E 00	0.387E 04	0.270E 12	0.840E 14	0.8356 15	
	56	495.0	0.000E 00	0.1088 04	0.158E 12	0.637E 14	0.713E 15	
	57	504.0	0.000E 00	0.298E 03	0.920E 11	0.480E 14	0.607E 15	
	58	513.0	0.000E 00	0.797E 02	0.5276 11	0.359E 14	0.514E 15	
	59	522.0	0.000E 00	0.2076 02	0.298E 11	0.267E 14	0.433E 15	
	60	531.0	0.000E 00	0.5288 01	0.1678 11	0.197E 14	0.363E 15	
	61	540.0	0.0000 00	0.130E 01	0.923E 10	0.1445 14	0.303E 15	
	63	558.0	0.0006 00	0.3156 00	0.3036 10	0.1056 14	0.2015 15	
(64	567.0	0.0005 00	0.1716-01	0.1455 10	0.5445 13	0.1716 15	
	65	576.0	0.000E 00	0.3835-02	0.7695 09	0.3886 13	0.1405 15	
	66	585.0	0.000E 00	0.837E-03	0.401E 09	0.275E 13	0.1145 15	
	67	594.0	0.000E 00	0.178E-03	0.207E 09	0.193E 13	0.927E 14	
	68	603.0	0.000E 00	0.3716-04	0.105E 09	0.135E 13	0.749E 14	
	69	612.0	0.000E 00	0.752E-05	0.5335 08	0.937E 12	0.602E 14	
$\langle \rangle$	70	621.0	0.000E 00	0.1486-05	0.266E 08	0.645E 12	0.482E 14	
	71	630.0	0.000E 00	0.286E-06	0.131E 08	0.442E 12	0.384E 14	
	72	639.0	0.000E 00	0.539E-07	0.639E 07	0.300E 12	0.304E 14	
	73	648.0	0.000E 00	0.990E-08	0.307E 07	0.203E 12	0.240E 14	
	14	657.0	0.0000 00	0.177E-08	0.146E 07	0.136E 12	0.189E 14	
	()	666.0	0.0000 00	0.3092-09	0.6902 06	0.907E 11	0.148E 14	
	77	684 0		0.9276-10	0.3218 06	0.0016 11	0.1152 14	
	78	693.0	0.0005.00	0.1416-11	0.4746 05	0.25956 11	0 4025 12	
(79	702.0	0.0006 00	0.224E - 12	0.3035 05	0.1676 11	0.5326 13	
	80	711.0	0.0005 00	0.3466-13	0.1355 05	0.1085 11	0.4075 13	
	81	720.0	0.000E 00	0.520E-14	0.594E 04	0.692E 10	0.310E 13	
(-	82	729.0	0.000E 00	0.764E-15	0.258E 04	0.441E 10	0.235E 13	1
	83	738.0	0.000E 00	0.109E-15	0.111E 04	0.278E 10	0.178E 13	
	84	747.0	0.000E 00	0.152E-16	0.473E 03	0.175E 10	0.134E 13	
	85	756.0	0.000E 00	0.208E-17	0.199E 03	0.109E 10	0.100E 13	
	86	765.0	0.000E 00	0.276E-18	0.828E 02	0.678E 09	0.749E 12	1-
								10

#8 7783.0 0.0000 00 0.00000 00 0.0000 00 0.0000		87	774.0	0.000E 00	0.000E 00	0.340E 02	0.417E 09	0.5568 12	
19 792.0 0.0006 00 0.0006 00 0.5387 00 0.3388 12 13 12 13 0.0006 00 0.0006 00 0.3386 00 0.3386 12 13 12.0 0.0006 00 0.0006 00 0.3386 00 0.3386 12 0.00386 11 14 137.0 0.0006 00 0.0006 00 0.0006 00 0.01176 00 0.0186 11 15 14.0 0.0006 00 0.0006 00 0.0006 00 0.01176 00 0.0168 11 195 15.6 0.0006 00 0.0006 00 0.0006 00 0.0128 07 0.1386 11 197 15.6 0.0006 00 0.0006 00 0.0128 07 0.1386 11 190 07.5 0.0006 00 0.0006 00 0.0128 07 0.1386 11 199 162.0 0.0006 00 0.0006 00 0.1386 00 0.1386 00 100 191.0 0.0006 00 0.0384 03 0.7586 06 0.7318 10		88	783.0	0.000E 00	0.000E 00	0.138E 02	0.255E 09	0.411E 12	
90 801.0 0.0000 00 0.0000 00 0.0336 00 0.0336 00 0.0336 00 0.0336 00 0.0336 00 0.0336 00 0.0336 00 0.0336 00 0.0336 00 0.0336 00 0.0336 00 0.0336 00 0.0336 00 0.0336 00 0.0336 00 0.0336 00 0.0336 00 0.0336 00 0.0336 00 0.0466 11 0.0000 00 0.0136 00 0.0466 01 0.0000 00 0.0336 00 0.0466 01 0.0000 00 0.0336 00 0.0466 01 0.0000 00 0.0336 00 0.0466 01 0.0000 00 0.0136 00 0.0000 00 0.0336 00 0.0466 01 0.0000 00 0.0136 00 0.0136 00 0.0136 00 0.0136 00 0.0146 00 0.0000 00 0.0136 00 0.0126 00		89	792.0	0.000E 00	0.000E 00	0.557E 01	0.155E 09	0.303E 12	
12 810-0 0.0000		90	801.0	0.000E 00	0.000E 00	0.2218 01	0.939E 08	0.222E 12	
25 922.0 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 <td< td=""><td></td><td>31</td><td>810.0</td><td>0.000E 00</td><td>0.000E 00</td><td>0.872E 00</td><td>0.564E 08</td><td>0.162E 12</td><td></td></td<>		31	810.0	0.000E 00	0.000E 00	0.872E 00	0.564E 08	0.162E 12	
3 937.0 0.0000 00 0.0000 00 0.6000 00 0.6376 07 0.6376 01<		92	819.0	0.000E 00	0.0000 00	0.3398 00	0.336E 08	0.1186 12	
33 044.0 0.00000 00 0.00000 00 0.00000 00 0.00000 00 0.00000 00 0.00000 00 0.00000 00 0.00000 00 0.00000 00 0.00000 00 0.00000 00 0.00000 00 0.00000 00 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.000000 0.00000		40	828.0	0.0000 00	0.000E 00	0.1305 00	0.1998 08	0.8548 11	
96 \$95:0 0.00010 0.000100 0.2384-02 0.2396-07 0.2364-11 98 875:0 0.000100 0.000100 0.2364-02 0.2396-07 0.2364-11 98 875:0 0.000100 0.000100 0.2364-02 0.2364-07 0.1226-07 0.1226-07 98 875:0 0.000100 0.000100 0.334-03 0.4286-06 0.1126-11 100 891:0 0.00010-00 0.334-03 0.4286-06 0.7916-10		34	844 0	0.0002 00	0.000E 00	0.4900-01	0.4975.07	0.6166 11	
97 194.00 0.000E 00		96	855.0	0.0005.00	0.0006 00	0.6065-02	0.2005.07	0 2145 11	
		90	864.0	0.0006 00	0.0002 00	0.2555-02	0.2205 07	0.2255 11	
		89	873.0	0.0005 00	0.0005 00	0.9295-02	0.1325 07	0.1506 11	
		99	882.0	0.0005 00	0.0000 00	0.3345-03	0.755E 06	0.1125 11	
		100	891.0	0.000E 00	0.000E 00	0.118E-03	0.428E 06	0.791E 10	
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RANGE =	0.100E 01 VALUE OF A	TOP = XISIS 0.0	0.100E 01 00E 00	BOTTOM =	0.000E 00	SCALE = 0.100E-01 PER STEP
DATA FO	R PLOTS					
	en en anten an				- Januar an margaritate bas	
STEP	POINTS 1	POINTS 2	POINTS 3	POINTS 4	POINTS 5	
1	0.000E 00	0.000E 00	0.000E 00	0.000E 00	0.000E 00	
2	0.253E-01	0.164E-02	0.3276-03	0.103E-03	0.000E 00	
3	0.175E 00	0.126E-01	0.257E-02	0.8226-03	0.338E-03	
4	0.464E 00	0.402E-01	0.845E-02	0.273E-02	0.113E-02	
5	0.7838 00	0.877E-01	0.193E-01	0.634E-02	0.264E-02	
6	0.987E 00	0.153E 00	0.359E-01	0.120E-01	0.507E-02	
77	0.100E 01	0.232E 00	0.584E-01	0.201E-01	0.858E-02	
8	0.844E 00	0.314E 00	0.865E-01	0.307E-01	0.132E-01	
9	0.607E 00	0.391E 00	0.119E 00	0.438E-01	0.1926-01	
10	0.3786 00	0.453E 00	0.1546 00	0.5928-01	0.265E-01	
11	0.206E 00	0.493E 00	0.1916 00	0.767E-01	0.350E-01	
12	0.9908-01	0.5098 00	0.227E 00	0.9582-01	0.4485-01	
1.3	0.4202-01	0.5000 00	0.2018 00	0.1765 00	0.5565-01	
	0.6336-03	0.4096 00	0.2896 00	0.1500 00	0.0735-01	
16	0.1605-02	0.3645 00	0.3295 00	0.1775 00	0.0296-01	
17	0.4305-03	0.3036 00	0.3375 00	0.1955 00	0.1065 00	
18	0-1036-03	0.2445 00	0.3395 00	0.2125 00	0.1195 00	
19	0.000E 00	0.1895 00	0.3336 00	0.226E 00	0.1325 00	
20	0.000E 00	0.142E 00	0.321E 00	0.238E 00	0.144E 00	
21	0.000E 00	0.103E 00	0.303E 00	0.246E.00	0.156F 00	
22	0.000E 00	0.725E-01	0.281E 00	0.252E 00	0.167E 00	
23	0.000E 00	0.495E-01	0.256E 00	0.254E 00	0.177E 00	
24	0.000E 00	0.327E-01	0.229E 00	0.253E 00	0.185E 00	
25	0.000E 00	0.210E-01	0.202E 00	0.250E 00	0.192E 00	
26	0.000E 00	0.130E-01	0.175E 00	0.2438 00	0.197E 00	
27	0.000E 00	0.792E-02	0.150E 00	0.234E 00	0.201E 00	
28	0.000E 00	0.466E-02	0.126E 00	0.2238 00	0.203E 00	
29	0.000E 00	0.266E-02	0.104E 00	0.211E 00	0.203E 00	
30	0.000E 00	0.148E-02	0.854E-01	0.197E 00	0.202E 00	
31	0.000E 00	0.800E-03	0.6888-01	0.182E 00	0.200E 00	
32	0.000E 00	0.421E-03	0.546E-01	0.167E 00	0.1958 00	
33	0.0008 00	0.215E-03	0.427E-01	0.151E 00	0.190E 00	
34	0.000E 00	0.107E-03	0.3308-01	0.136E 00	0.1848 00	
30	0.0000 00	0.0000 00	0.1000-01	0.1228 00	0.1/65 00	
27	0.0000 00	0.0000 00	0.1405-01	0.9475-01	0.1605 00	
20	0.0005 00	0.0000 00	0.1025-01	0.8225-01	0.1606 00	
30	0.000F 00	0.000E 00	0.740F-02	0.7105-01	0.1415 00	
40	0.000E 00	0.000E 00	0.5285-02	0.6076-01	0.1316 00	
41	0.000F 00	0.000E 00	0.3725-02	0.5165-01	0.121E 00	
42	0.000E 00	0.000E 00	0.2586-02	0.434E-01	0.111E 00	
43	0.000E 00	0.000E 00	0.1776-02	0.362E-01	0.102E 00	
44	0.000E 00	0.000E 00	0.1208-02	0.3006-01	0.930E-01	
45	0.000E 00	0.000E 00	0.807E-03	0.2478-01	0.842E-01	
46	0.000E 00	0.000E 00	0.533E-03	0.2028-01	0.7576-01	
47	0.000E 00	0.000E 00	0.348E-03	0.163E-01	0.678E-01	
48	0.000E 00	0.000E 00	0.225E-03	0.131E-01	0.603E-01	
49	0.000E 00	0.000E 00	0.143E-03	0.105E-01	0.534E-01	
50	0.000E 00	0.000E 00	0.000E 00	0.832E-02	0.470E-01	
51	0.000E 00	0.000E 00	0.000E 00	0.654E-02	0.412E-01	A server at the se
5.2	0.000E 00	0.000F 00	0.000E 00	0.5115-02	0.3506-01	

53 0.000E 0.000E 0.000E 0.306E-02 0.302E-01 54 0.000E 0 0.000E 0 0.302E-02 0.202E-01 55 0.000E 0 0.000E 0 0.302E-02 0.202E-01 57 0.000E 0 0.000E 0 0.000E 0 0.202E-01 57 0.000E 0 0.000E 0 0.000E 0 0.142E-01 58 0.000E 0 0.000E 0 0.000E 0 0.126E-01 59 0.000E 0 0.000E 0 0.000E 0 0.126E-01 60 0.000E 0 0.000E 0 0.400E-03 0.484E-02 61 0.000E 0 0.000E 0 0.400E-03 0.480E-02 62 0.000E 0 0.000E 0 0.400E-03 0.480E-02 63 0.000E 0 0.000E 0 0.000E-03 0.400E-03 64 </th <th>*</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th>	*						
53 0.0006 00.0006 <							
54 0.0006 00 0.0007 00.2357-02 0.2357-01 55 0.0007 00 0.0007 00 0.2357-01 56 0.0007 00 0.0007 00 0.2357-01 57 0.0007 00 0.0007 00 0.1357-01 57 0.0007 00 0.0007 00 0.1427-01 59 0.0007 00 0.0007 00 1.1327-02 0.1427-01 60 0.0007 00 0.0007 00 1.1327-02 0.14267-01 61 0.0007 00 0.0007 0.0007 0.0007 0.0007 0.0007 63 0.0007 00 0.0007		53	0.000E 00	0.000E 00	0.000E 00	0.396E-02	0.3126-01
55 0.00000 0.000000 0.00000		54	0.000E 00	0.000E 00	0.000E 00	0.305E-02	0.269E-01
56 0.0006 00 0.0006 00 0.1086-01 57 0.0006 00 0.0006 00 0.1336-02 0.1486-01 58 0.0006 00 0.0006 00 0.0006 00 0.1206-01 60 0.0006 00 0.0006 00 0.0006 00 0.4406-02 61 0.0006 00 0.0006 00 0.4406-02 0.4406-02 62 0.0006 00 0.0006 00 0.4406-02 0.5776-02 63 0.0006 00 0.0006 00 0.1216-03 0.4776-02 64 0.0006 00 0.0006 00 0.1216-03 0.4776-02 64 0.0006 00 0.0006 00 0.0006 00 0.1286-02 67 0.0006 00 0.0006 00 0.1386-02 0.1286-02 67 0.0006 00 0.0006 00 0.1386-02 0.1776-02 71		55	0.000E 00	0.000E 00	0.000E 00	0.233E-02	0.231E-01
$\begin{array}{c} 57 & 0.0006 & 00 & 0.0006 & 00 & 0.0076 & 00 & 0.0976 & 00 & 0.1426 & -01 \\ 59 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.9976 & 00 & 0.1426 & -01 \\ 60 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.9976 & 00 & 0.0006 & -01 \\ 61 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.9976 & -02 \\ 62 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.2916 & -02 \\ 64 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.2916 & -02 \\ 65 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.2916 & -02 \\ 65 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.1076 & -02 \\ 66 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.1076 & -02 \\ 66 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.2716 & -02 \\ 66 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.2716 & -02 \\ 66 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.27716 & -02 \\ 66 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.27716 & -02 \\ 77 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.27716 & -02 \\ 77 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.1076 & -02 \\ 77 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.1076 & -02 \\ 77 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.1076 & -02 \\ 77 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 \\ 77 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 \\ 77 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 \\ 77 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 \\ 77 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 \\ 77 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 \\ 77 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 \\ 77 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 \\ 77 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 \\ 77 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 \\ 77 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 \\ 77 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 \\ 78 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 \\ 79 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 \\ 79 & 0.0006 & 00$		56	0.000E 00	0.000E 00	0.000E 00	0.176E-02	0.1985-01
$ \begin{array}{c} 58 \\ 59 \\ 0.00000 $		57	0.000E 00	0.000E 00	0.000E 00	0.133E-02	0.168E-01
59 0.0006 00 0.0006 00 0.1006-01 61 0.0006 00 0.0006 00 0.0006 00 0.0006 62 0.0006 00 0.0006 00 0.0006 00 0.0006 00 0.0006 00 0.0006 00 0.0006 <t< td=""><td></td><td>58</td><td>0.000E 00</td><td>0.000E 00</td><td>0.000E 00</td><td>0.997E-03</td><td>0.1426-01</td></t<>		58	0.000E 00	0.000E 00	0.000E 00	0.997E-03	0.1426-01
00 0.0006 0.0006 0.0006		59	0.000E 00	0.000E 00	0.000F 00	0.740E-03	0.1205-01
61 0.00000 0.000000 0.000000 0.4000000 0.4000000 0.4000000 0.4000000 0.4000000 0.4000000 0.4000000 0.4000000 0.4000000 0.400000000 0.400000000 0.400000000 0.400000000000000000000000000000000000		60	0.000E 00	0.000E 00	0.000E 00	0.546E-03	0.1005-01
62 0.00000 0.00000 0.0		61	0.000F 00	0.000F 00	0.000F 00	0.400E-03	0.8405-02
63 0.4000E 00 0.2102=03 0.377E=02 64 0.4000E 00 0.4000E 0.400E		62	0.000E 00	0.000E 00	0.000E 00	0.291E-03	0.698E-02
64 0.000E 00 0.000E 00 0.151E-03 0.347E-02 65 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.31E-02 66 0.000E 00 0.000E 00 0.000E 00 0.207E-02 68 0.000E 00 0.000E 00 0.000E 00 0.207E-02 70 0.000E 00 0.000E 00 0.000E 00 0.137E-02 71 0.000E 00 0.000E 00 0.000E 00 0.137E-02 71 0.000E 00 0.000E 00 0.000E 00 0.137E-02 71 0.000E 00 0.000E 00 0.000E 00 0.137E-02 72 0.000E 00 0.000E 00 0.000E 00 0.137E-02 73 0.000E 00 0.000E 00 0.000E 00 0.000E 0.000E 0.000E		63	0.000F 00	0.000F 00	0.000F 00	0.2105-03	0.5776-02
6.6 0.000E 00 0.000E <t< td=""><td>,</td><td>64</td><td>0.0005 00</td><td>0.000F 00</td><td>0.0006 00</td><td>0.1516-03</td><td>0.4746-02</td></t<>	,	64	0.0005 00	0.000F 00	0.0006 00	0.1516-03	0.4746-02
66 0.000E 00 0.000E 0.000E 00 0.000E		65	0.0005 00	0.0005 00	0.0000 00	0.1075-03	0.3885-02
67 0.0002 00 0.0002 00 0.0002 00 0.257E-02 66 0.0002 00 0.0002 00 0.0002 00 0.207E-02 70 0.0002 00 0.0002 00 0.0002 00 0.137E-02 71 0.0002 00 0.0002 00 0.137E-02 72 0.0002 00 0.0002 00 0.4662 0.0002 72 0.0002 00 0.0002 0 0.4662 0.0002 73 0.0002 00 0.0002 0 0.4662 0.0002 74 0.0002 00 0.0002 00 0.2255 0.0002 74 0.0002 00 0.0002 00 0.2255 0.0002 75 0.0002 00 0.0002 00 0.2456 0.0002 0.0002 0.0002 0.0002 0.0002 0.0002 0.0002 0.0002 0.0002 0.0002 0.0002 0.0002		66	0.0005 00	0.0005 00	0.0005 00	0.000E 00	0.3176-02
3 0 0.0000 00 0.0000 00 0.2007 <th0.2007< th=""> 0.2007 0.</th0.2007<>		67	0.0000 00	0.0005 00	0.0000 00	0.0006 00	0.2575-02
ag 0.0002 00 0.0002 <th< td=""><td></td><td>68</td><td>0.000E 00</td><td>0.000E 00</td><td>0.0005 00</td><td>0.0005 00</td><td>0.2076-02</td></th<>		68	0.000E 00	0.000E 00	0.0005 00	0.0005 00	0.2076-02
03 0 <th0< th=""> 0 <th0< th=""> <th0< th=""></th0<></th0<></th0<>		40	0.0006 00	0.0005 00	0.0000 00	0.0000 00	0.1676-02
10 0.0000 0.0000 0.0000 0.0000 0.00000		70	0.0000 00	0.0005 00	0.0000 00	0.0000 00	0 1336-02
11 0.0000 00 0.0000 00 0.0000 00 0.0000 00 0.0000 00 0.0000 00 0.0000 00 0.0000 00 0.0000 00 0.0000 00 0.0000 00 0.0000 00 0.0000 00 0.0000 0.0000 00 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000		70	0.0000 00	0.0000 00	0.0000 00	0.0000 00	0.1045-02
72 0.000E 000 0.000E 00		72	0.0000 00	0.0000 00	0.0002 00	0.0000 00	0.1066-02
73 0.000E 00 <		12	0.0000 00	0.0000 00	0.0002 00	0.0000 00	0.8452-03
74 0.0000 00 <		71	0.0000 00	0.0000 00	0.0000 00	0.000E 00	0.6682-03
75 0.00000 0.00000 0.00000 0.00000 0.0000000		14	0.0000 00	0.00000 00	0.0000 00	0.000E 00	0.5252-03
76 0.0006 00 0.0006 00 0.0006 00 0.0006 00 0.246E-03 77 0.0006 00 0.0006 00 0.0006 00 0.147E-03 80 0.0006 00 0.0006 00 0.0006 00 0.147E-03 81 0.0006 00 0.0006 00 0.0006 00 0.0006 00 0.0006 00 82 0.0006 00 0.0006 00 0.0006 00 0.0006 00 0.0006 00 83 0.0006 00 0.0006 00 0.0006 00 0.0006 00 0.0006 00 84 0.0006 00 0.0006 00 0.0006 00 0.0006 00 0.0006 00 84 0.0006 00 0.0006 00 0.0006 00 0.0006 00 0.0006 00 84 0.0006 00 0.0006 00 0.0006 00 0.0006 00 0.0006 00 84 0.0006 00 0.0006 00 0.0006 00 0.0006 00 0.0006 00 88 0.0006 00 0.0006 00 0.0006 00 0.0006 00 0.0006 00 90 0.0006 00 0.0006 00 0.0006 00 0.0006 00 0.0006 00 91 0.0006 00 0.0006 00 0.0006 00 0.0006 00 0.0		15	0.000E 00	0.00000 00	0.0000000	0.000E 00	0.411E=03
77 0.000E 00 <		76	0.000E 00	0.000E 00	0.000E 00	0.000E 00	0.320E-03
78 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.192E-03 79 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.113E-03 81 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 82 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 83 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 84 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 86 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 88 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 88 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 90 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 92 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 93 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 94 0.000E 00 0.000E 00 0.0		11	0.000E 00	0.000E 00	0.000E 00	0.000E 00	0.248E-03
79 0.000E 00 <		78	0.000E 00	0.000E 00	0.0008 00	0.000E 00	0.192E-03
80 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.113E-03 81 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 82 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 83 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 84 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 85 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 86 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 88 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 90 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 91 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 92 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00		79	0.000E 00	0.000E 00	0.000E 00	0.000E 00	0.147E-03
81 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 82 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 83 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 84 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 85 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 86 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 87 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 88 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 90 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 91 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 93 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.		80	0.000E 00	0.000E 00	0.000E 00	0.0008 00	0.113E-03
82 0.000E 00 0.000E 00 0.000E 00 0.000E 00 83 0.000E 00 0.000E 00 0.000E 00 0.000E 00 84 0.000E 00 0.000E 00 0.000E 00 0.000E 00 85 0.000E 00 0.000E 00 0.000E 00 0.000E 00 86 0.000E 00 0.000E 00 0.000E 00 0.000E 00 87 0.000E 00 0.000E 00 0.000E 00 0.000E 00 88 0.000E 00 0.000E 00 0.000E 00 0.000E 00 90 0.000E 00 0.000E 00 0.000E 00 0.000E 00 91 0.000E 00 0.000E <td< td=""><td></td><td>81</td><td>0.000E 00</td><td>0.000E 00</td><td>0.000E 00</td><td>0.000E 00</td><td>0.000E 00</td></td<>		81	0.000E 00	0.000E 00	0.000E 00	0.000E 00	0.000E 00
83 0.000E 00 0.000E 00 0.000E 00 84 0.000E 00 0.000E 00 0.000E 00 0.000E 00 85 0.000E 00 0.000E 00 0.000E 00 0.000E 00 86 0.000E 00 0.000E 00 0.000E 00 0.000E 00 87 0.000E 00 0.000E 00 0.000E 00 0.000E 00 88 0.000E 00 0.000E 00 0.000E 00 0.000E 00 90 0.000E 00 0.000E 00 0.000E 00 0.000E 00 91 0.000E 00 0.000E 00 0.000E 00 0.000E 00 92 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 93 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00		82	0.000E 00	0.000E 00	0.000E 00	0.000E 00	0.000E 00
84 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 85 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 86 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 87 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 88 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 90 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 91 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 92 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 93 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 94 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 94 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 96 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 97 0.000E 00 0.000E 00 0.0		83	0.000E 00	0.000E 00	0.000E 00	0.000E 00	0.000E 00
85 0.000E 00 0.000E 00 0.000E 00 86 0.000E 00 0.000E 00 0.000E 00 0.000E 00 87 0.000E 00 0.000E 00 0.000E 00 0.000E 00 88 0.000E 00 0.000E 00 0.000E 00 0.000E 00 90 0.000E 00 0.000E 00 0.000E 00 0.000E 00 91 0.000E 00 0.00		84	0.000E 00	0.000E 00	0.000E 00	0.000E 00	0.000E 00
86 0.000E 00 0.000E 00 0.000E 00 0.000E 00 87 0.000E 00 0.000E 00 0.000E 00 0.000E 00 88 0.000E 00 0.000E 00 0.000E 00 0.000E 00 99 0.000E 00 0.000E 00 0.000E 00 0.000E 00 90 0.000E 00 0.000E 00 0.000E 00 0.000E 00 91 0.000E 00 0.000E 00 0.000E 00 0.000E 00 92 0.000E 00 0.000E 00 0.000E 00 0.000E 00 93 0.000E 00 0.000E 00 0.000E 00 0.000E 00 94 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 94 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00		85	0.000E 00	0.000E 00	0.000E 00	0.000E 00	0.000E 00
87 0.000E 00 0.000E 00 0.000E 00 88 0.000E 00 0.000E 00 0.000E 00 0.000E 00 90 0.000E 00 0.000E 00 0.000E 00 0.000E 00 91 0.000E 00 0.000E 00 0.000E 00 0.000E 00 92 0.000E 00 0.000E 00 0.000E 00 0.000E 00 91 0.000E 00 0.000E 00 0.000E 00 0.000E 00 92 0.000E 00 0.000E 00 0.000E 00 0.000E 00 93 0.000E 00 0.000E		86	0.000E 00	0.000E 00	0.000E 00	0.000E 00	0.000E 00
88 0.000E 00 0.000E 00 0.000E 00 0.000E 00 90 0.000E 00 0.000E 00 0.000E 00 0.000E 00 91 0.000E 00 0.000E 00 0.000E 00 0.000E 00 92 0.000E 00 0.000E 00 0.000E 00 0.000E 00 93 0.000E 00 0.000E 00 0.000E 00 0.000E 00 94 0.000E 00 0.000E 00 0.000E 00 0.000E 00 94 0.000E 00 0.000E 00 0.000E 00 0.000E 00 94 0.000E 00 0.000E 00 0.000E 00 0.000E 00 95 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00 97 0.000E 00 0.000E 00 0.000E 00 0.000E 00 0.000E 00		87	0.000E 00	0.000E 00	0.000E 00	0.000E 00	0.000E 00
89 0.000E 00 0.000E 00 0.000E 00 0.000E 00 90 0.000E 00 0.000E 00 0.000E 00 0.000E 00 91 0.000E 00 0.000E 00 0.000E 00 0.000E 00 92 0.000E 00 0.000E 00 0.000E 00 0.000E 00 93 0.000E 00 0.000E 00 0.000E 00 0.000E 00 94 0.000E 00 0.000E 00 0.000E 00 0.000E 00 95 0.000E 00 0.000E 00 0.000E 00 0.000E 00 96 0.000E 00 0.000E 00 0.000E 00 0.000E 00 97 0.000E 00 0.000E 00 0.000E 00 0.000E 00 98 0.000E 00 0.000E 00 0.000E 00 0.000E 00 99 0.000E 00 <td></td> <td>88</td> <td>0.000E 00</td> <td>0.000E 00</td> <td>0.000E 00</td> <td>0.000E 00</td> <td>0.000E 00</td>		88	0.000E 00	0.000E 00	0.000E 00	0.000E 00	0.000E 00
90 0.000E 00 0.000E 00 0.000E 00 0.000E 00 91 0.000E 00 0.000E 00 0.000E 00 0.000E 00 92 0.000E 00 0.000E 00 0.000E 00 0.000E 00 93 0.000E 00 0.000E 00 0.000E 00 0.000E 00 94 0.000E 00 0.000E 00 0.000E 00 0.000E 00 95 0.000E 00 0.000E 00 0.000E 00 0.000E 00 96 0.000E 00 0.000E 00 0.000E 00 0.000E 00 97 0.000E 00 0.000E 00 0.000E 00 0.000E 00 98 0.000E 00 0.000E 00 0.000E 00 0.000E 00 99 0.000E 00 0.000E 00 0.000E 00 0.000E 00 99 0.000E 00 <td></td> <td>89</td> <td>0.000E 00</td> <td>0.000E 00</td> <td>0.000E 00</td> <td>0.000E 00</td> <td>0.000E 00</td>		89	0.000E 00	0.000E 00	0.000E 00	0.000E 00	0.000E 00
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TYPE OF ATOM IS RB MASS= 0.14198E-21GRAMS TEMPERATURE= 450.0DEG. K.

ACCORDING TO MAXWELLIAN DISTRIBUTION, VMP=(2KT/M)**.5, AV=(8KT/3.141M)**.5, RMSV=(3KT/M)**.5

VMP= 0.29580E 05CM/SEC AV= 0.33381E 05CM/SEC RMSV= 0.36228E 05CM/SEC

ACCORDING TO EFFUSIVE FLOW DISTRIBUTION, VMP=(3KT/M)**.5, AV=.75(2*3.141KT/M)**.5, RMSV=(KT/M)**.5

VMP= 0.36228E 05CM/SEC AV= 0.39319E 05CM/SEC RMSV= 0.20916E 05CM/SEC

TIME= 0.138E-02SEC DISTANCE= 0.500E 02CM FOR POINTS 1

TIME= 0.276E-02SEC DISTANCE= 0.100E 03CM FOR POINTS 2

TIME= 0.414E-02SEC DISTANCE= 0.150E 03CM FOR POINTS 3

TIME= 0.552E-02SEC DISTANCE= 0.200E 03CM FOR POINTS 4

TIME= 0.690E-02SEC DISTANCE= 0.250E 03CM FOR POINTS 5

PLOT OF I VS S ACCORDING TO THE EQUATION I=C(S**3/T**4)*E**(-BS**2/T**2)

	INCRE	MENT ALONG X-AXIS=	9.0CM,	CON	STANT T	IME	UNNORMA	LIZED	DATA				
	STEP	DISTANCE(IN CM)	POINTS	1	POINTS	2	POINTS	3	POINTS	4	POINTS	5	
	1	0.0	0.000E	00	0.000E	00	0.000E	00	0.000E	00	0.000E	00	
	2	9.0	0.191E	15	0.124E	14	0.2468	13	0.782E	12	0.320E	12	
	3	18.0	0.132E	16	0.957E	14	0.194E	14	0.620E	13	0.255E	13	
-	4	27.0	0.350E	16	0.303E	15	0.638E	14	0.206E	14	0.853E	13	
	5	36.0	0.590E	16	0.661E	15	0.145E	15	0.478E	14	0.199E	14	
	6	45.0	0.745E	16	0.115E	16	0.270E	15	0.909E	14	0.382E	14	
	7	54.0	0.754E	16	0.175E	16	0.441E	15	0.151E	15	0.647E	14	
	8	63.0	0.636E	16	0.237E	16	0.653E	15	0.231E	15	0.1008	15	а. -
	9	72.0	0.458E	16	0.295E	16	0.899E	15	0.330E	15	0.145E	15	
	10	81.0	0.2858	16	0.342E	16	0.116E	16	0.447E	15	0.200E	15	
	11	90.0	0.155E	16	0.372E	16	0.144E	16	0.579E	15	0.264E	15	
	12	99.0	0.747E	15	0.384E	16	0.1716	16	0.723E	15	0.338E	15	
	13	108.0	0.317E	15	0.377E	16	0.1968	16	0.875E	15	0.419E	15	
	14	117.0	0.119E	15	0.354E	16	0.218E	16	0.103E	16	0.508E	15	
	15	126.0	0.402E	14	0.318E	16	0.236E	16	0.118E	16	0.602E	15	
	16	135.0	0.120E	14	0.275E	16	0.248E	16	0.133E	16	0.700E	15	
	17	144.0	0.325E	13	0.229E	16	0.255E	16	0.147E	16	0.800E	15	
	18	153.0	0.784E	12	0.184E	16	0.255E	16	0.160E	16	0.900E	15	
	19	162.0	0.169E	12	0.142E	16	0.251E	16	0.171E	16	0.998E	15	
	20	171.0	0.330E	11	0.107E	16	0.242E	16	0.179E	16	0.109E	16	
	21	180.0	0.580E	10	0.778E	15	0.228E	16	0.186E	16	0.118E	16	
	22	189.0	0.915E	09	0.547E	15	0.212E	16	0.190E	16	0.126E	16	
	23	198.0	0.130E	09	0.373E	15	0.193E	16	0.192E	16	0.133E	16	
	24	207.0	0.167E	08	0.247E	15	0.173E	16	0.191E	16	0.139E	16	
	25	216.0	0.193E	07	0.158E	15	0.152E	16	0.188E	16	0.145E	16	
	26	225.0	0.2016	06	0.988E	14	0.132E	16	0.183E	16	0.149E	16	
	27	234.0	0.190E	05	0.598E	14	0.113E	16	0.177E	16	0.151E	16	

	20	242.0	0 1/25 0/	0 2010 14	0 0505	15	0 1405 14	0 1525 14	
	28	243.0	0.1525 04	0.3516 14	0.7905	15	0.1685 16	0 1535 16	
	20	252.0	0.1246 03	0.2018 14	0.1096	15	0.1596 10	0 1626 14	
	21	270.0	0.547E 00	0.6045 13	0.5195	15	0.137E 16	0.1505 16	
C	32	279.0	0.3116-01	0.3175 13	0.4125	15	0.126F 16	0.147E 16	
31 2	33	288.0	0.160E-02	0.162E 13	0.3225	15	0.114E 16	0.1438 16	
	34	297.0	0.7476-04	0.809E 12	0.249F	15	0.103E 16	0.1398 16	
(	35	306.0	0-3146-05	0.392E 12	0.189F	15	0.921E 15	0.1338 16	
	36	315.0	0.120E-06	0.185E 12	0.142E	15	0.814E 15	0.127E 16	
	37	324.0	0.414E-08	0.849E 11	0.105E	15	0.714E 15	0.120E 16	
(	38	333.0	0.129E-09	0.380E 11	0.7736	14	0.621E 15	0.113E 16	
	39	342.0	0.366E-11	0.165E 11	0.559E	14	0.536E 15	0.106E 16	
	40	351.0	0.939E-13	0.701E 10	0.398E	14	0.458E 15	0.991E 15	
	41	360.0	0.218E-14	0.290E 10	0.2808	14	0.389E 15	0.917E 15	
	42	369.0	0.458E-16	0.1168 10	0.195E	14	0.327E 15	0.843E 15	
	43	378.0	0.872E-18	0.457E 09	0.134E	14	0.273E 15	0.772E 15	
(	44	387.0	0.000E 00	0.174E 09	0.909E	13	0.227E 15	0.7028 15	
	45	396.0	0.000E 00	0.651E 08	0.609E	13	0.186E 15	0.635E 15	
	46	405.0	0.000E 00	0.236E 08	0.4028	13	0.152E 15	0.571E 15	
	47	414.0	0.0008 00	0.835E 07	0.2638	13	0.123E 15	0.511E 15	
-	48	423.0	0.000E 00	0.287E 07	0.169E	13	0.993E 14	0.455E 15	
	49	432.0	0.000E 00	0.966E 06	0.108E	13	0.792E 14	0.4038 15	
(	50	441.0	0.000E 00	0.316E 06	0.682E	12	0.628E 14	0.355E 15	
	51	450.0	0.000E 00	0.100E 06	0.425E	12	0.494E 14	0.311E 15	
	52	459.0	0.0000 00	0.314E 05	0.261E	12	0.385E 14	0.2716 15	
	53	468.0	0.0002 00	0.952E 04	0.1585	12	0.2998 14	0.2356 15	
	24	4//.0	0.0002 00	0.2812 04	0.9546	11	0.2305 14	0.2036 15	
	22	480.0	0.0002 00	0.3115 03	0.3000	11	0.1226 14	0.1405 15	
	20	492.0	0.0002 00	0.2286 03	0.3326	11	0.1335 14	0.1276 15	
	27	504.0	0.0002 00	0.0246 02	0.1926	11	0.1000 14	0.1076 15	
	<u> </u>	522.0	0.0000 00	0.4355 01	0.4745	10	0.6505 13	0.0065.16	
	60	522.0	0.0005 00	0.1106 01	0.3495	10	0 6126 13	0.7605 14	
	61	540.0	0.0005 00	0.2736 00	0.1935	10	0.3026 13	0.6345 14	
	62	549.0	0.0005 00	0.6616-01	0.1055	10	0.210F 13	0.5265 14	
	63	558.0	0.000F 00	0.1556-01	0.571F	09	0.158E 13	0.435F 14	
	64	567.0	0.000E 00	0.357E-02	0.3056	09	0.114E 13	0.358E 14	
Ca	65	576.0	0.000E 00	0.802E-03	0.1618	09	0.812E 12	0.293E 14	
	66	585.0	0.000E 00	0.175E-03	0.841E	08	0.575E 12	0.239E 14	
entellabilitiones una functiones en passimentana	67	594.0	0.000E 00	0.373E-04	0.434E	80	0.404E 12	0.1946 14	
(	68	603.0	0.000E 00	0.776E-05	0.221E	08	0.282E 12	0.156E 14	
	69	612.0	0.000E 00	0.157E-05	0.111E	80	0.196E 12	0.126E 14	
	70	621.0	0.000E 00	0.311E-06	0.556E	07	0.135E 12	0.1008 14	
	71	630.0	0.000E 00	0.600E-07	0.274E	07	0.925E 11	0.804E 13	
	72	639.0	0.000E 00	0.112E-07	0.133E	07	0.629E 11	0.638E 13	
	73	648.0	0.000E 00	0.207E-08	0.644E	06	0.424E 11	0.504E 13	
	74	657.0	0.000E 00	0.371E-09	0.306E	06	0.285E 11	0.396E 13	
	75	666.0	0.000E 00	0.647E-10	0.144E	06	0.190E 11	0.310E 13	
	76	675.0	0.000E 00	0.110E-10	0.673E	05	0.125E 11	0.241E 13	
	11	684.0	0.000E 00	0.183E-11	0.3098	05	0.827E 10	0.1872 13	
	18	693.0	0.0000 00	0.297E-12	0.141E	05	0.5408 10	0.144E 13	
	19	702.0	0.0000 00	0.4096-13	0.0345	04	0.3006 10	0.0526 12	
	<u>au</u>	720.0	0.0000 00	0.1005-14	0.1245	40	0.1455 10	0 4505 12	
	C 1	720.0	0.0002 00	0.1405-14	0.5416	03	0.0226 00	0 403 12	
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	0 <b>7</b>	756.0	0.0006 00	0.4365-18	0.4165	02	0.2285 00	0.2105 12	
	86	765-0	0.0005 00	0.5795-19	0.1736	02	0.141E 09	0.1565 12	
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	88	783.0	0.000E 00	0.000E 00	0.290E 01	0.535E 08	0.861E 11	
(	89	792.0	0.000E 00	0.000E 00	0.116E 01	0.325E 08	0.634E 11	
	90	801.0	0.000E 00	0.000E 00	0.4635 00	0.196E 08	0.465E 11	
C	92	819.0	0.000E 00	0.000E 00	0.7096-01	0.1186 08	0.339E 11 0.247E 11	
	93	828.0	0.000E 00	0.000E 00	0.273E-01	0.417E 07	0.178E 11	
<u>.</u>	94	837.0	0.000E 00	0.000E 00	0.103E-01	0.245E 07	0.128E 11	
	95	846.0	0.000E 00	0.000E 00	0.390E-02	0.143E 07	0.926E 10	
	97	864.0	0.000E 00	0.0000 00	0.5346-03	0.4836 06	0.4716 10	
( <u> </u>	98	873.0	0.000E 00	0.000E 00	0.1946-03	0.277E 06	0.334E 10	
	99	882.0	0.000E 00	0.000E 00	0.6995-04	0.158E 06	0.235E 10	
	100	891.0	0.000E 00	0.000E 00	0.249E-04	0.896E 05	0.165E 10	
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	RANGE =	0.100E 01 VALUE OF A	TOP =	0.100E 01 00E 00	BOTTOM =	0.000E 00	SCALE =	0.100E-01 PER STEP	
1	DATA FOR	PLOTS							
	STEP	POINTS 1	POINTS 2	POINTS 3	POINTS 4	POINTS 5			
	1	0.000E 00	0.000E 00	0.000E 00	0.000E 00	0.000E 00			
	2	0.253E-01	0.164E-02	0.3275-03	0.103E-03	0.000E 00			
	3	0.175E 00	0.126E-01	0.2576-02	0.822E-03	0.338E-03			
	4	0.464E 00	0.402E-01	0.845E-02	0.273E-02	0.113E-02			
	5	0.783E 00	0.877E-01	0.193E-01	0.634E-02	0.264E-02			
	6	0.987E 00	0.153E 00	0.359E-01	0.1208-01	0.507E-02			
	7	0.100E 01	0.232E 00	0.584E-01	0.201E-01	0.858E-02			•
	8	0.844E 00	0.314E 00	0.865E-01	0.307E-01	0.132E-01			
	9	0.607E 00	0.391E 00	0.1196 00	0.438E-01	0.192E-01			
	10	0.378E 00	0.453E 00	0.154E 00	0.592E-01	0.265E-01			
	11	0.2068 00	0.493E 00	0.191E 00	0.767E-01	0.350E-01			
	12	0.990E-01	0.509E 00	0.227E 00	0.958E-01	0.448E-01			
	13	0.420E-01	0.500E 00	0.261E 00	0.116E 00	0.556E-01			
	14	0.1582-01	0.469E 00	0.289E 00	0.136E 00	0.673E-01			
	15	0.533E-02	0.4226 00	0.313E 00	0.157E 00	0.798E-01			
	16	0.1606-02	0.364E 00	0.3298 00	0.177E 00	0.928E-01			
	17	0.430E-03	0.303E 00	0.3378 00	0.1958 00	0.106E 00			
	18	0.103E-03	0.244E 00	0.339E 00	0.2128 00	0.119E 00			
	19	0.0002 00	0.1898 00	0.333E 00	0.226E 00	0.132E 00			
	20	0.000E 00	0.142E 00	0.321E 00	0.238E 00	0.144E 00			
	21	0.00000 00	0.103E 00	0.303E 00	0.2468 00	0.1568 00		**	
	22	0.00000 00	0.7252-01	0.2818 00	0.2528 00	0.1678 00			
	23	0.0000 00	0.4956-01	0.2568 00	0.2548 00	0.1778 00			
	24	0.00000 00	0.3276-01	0.2298 00	0.2538 00	0.1856 00			
	22	0.0000 00	0.2100-01	0.2028 00	0.2502 00	0.1928 00	and a subject to not other of the full of the subject of the factors of the factors of the factors of the factor		
	20	0.0002 00	0.1906-01	0.1752 00	0.2436 00	0.1978 00			
	20	0.0000 00	0.1926-02	0.1365.00	0.2346 00	0.2016 00			
	20	0.0000 00	0.3465-02	0.1268 00	0.2235 00	0.2036 00			
	30	0.0005 00	0.1495-02	0.9545-01	0.1076.00	0.2036 00			
	21	0.0000 00	0.8006-03	0.6995-01	0.1976 00	0.1005 00			
	32	0.0005 00	0.4215-03	0.5465-01	0.1675.00	0.1956 00			
	22	0.0005 00	0.2155-03	0.4276-01	0 1515 00	0.1905 00			
	34	0.000E 00	0.1076-03	0.3305-01	0.1365 00	0.1965 00			
	24	0.0005 00	0.0006.00	0.2515-01	0.1226.00	0.1745 00			
	36	0.0005 00	0.0006 00	0.1885-01	0.107E 00	0.1685 00			
	37	0.0005 00	0.000F 00	0-1405-01	0.9476-01	0.1605 00			
	38	0.000E 00	0.000E 00	0.1025-01	0.8235-01	0.1505 00			
	39	0.0005 00	0.000F 00	0.7405-02	0.7106-01	0.1415 00			
	40	0.0005 00	0.0005 00	0.5285-02	0.6075-01	0.1315 00			
	41	0.000E 00	0.000F 00	0.3725-02	0.5165-01	0.1216 00			
	42	0.0005 00	0.000E 00	0.2585-02	0.4345-01	0.1116 00			
	43	0.0008 00	0.000F 00	0.1775-02	0.3626-01	0.102E 00			
	44	0.0005 00	0.000E 00	0.1205-02	0.300F-01	0.9305-01			
	45	0.000E 00	0.000E 00	0.807E-03	0.247E-01	0.8425-01			
	46	0.000E 00	0.000E 00	0.533E-03	0.202E-01	0.7576-01			
	47	0.0000 00	0.000E 00	0.348E-03	0.163E-01	0.678E-01			
_	48	0.000E 00	0.000E 00	0.2256-03	0.1315-01	0.603E-01			
	49	0.000E 00	0.000E 00	0.1436-03	0.105E-01	0.534E-01			
	50	0.000E 00	0.000E 00	0.000E 00	0.832E-02	0.470E-01			
	51	0.000E 00	0.000E 00	0.000E 00	0.654E-02	0.4125-01			
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	52	0.000E 00	0.000E 00	0.000E 00	0.511E-02	0.359E-01			

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	53	0.000E 00	0.000E 00	0.000E 00	0.396E-02	0.312E-01
	54	0.0008 00	0.000E 00	0.000E 00	0.305E-02	0.269E-01
	55	0.000E 00	0.000E 00	0.000E 00	0.233E-02	0.231E-01
	56	0.000E 00	0.000E 00	0.000E 00	0.1765-02	0.198E-01
	57	0.0008 00	0.000E 00	0.000E 00	0.133E-02	0.168E-01
	58	0.000E 00	0.000E 00	0.000E 00	0.997E-03	0.142E-01
	59	0.000E 00	0.000E 00	0.000E 00	0.740E-03	0.120E-01
	60	0.000E 00	0.000E 00	0.000E 00	0.546E-03	0.100E-01
	61	0.000E 00	0.000E 00	0.000E 00	0.400E-03	0.840E-02
	62	0.000E 00	0.000E 00	0.000E 00	0.291E-03	0.698E-02
	63	0.000E 00	0.000E 00	0.000E 00	0.210E-03	0.577E-02
	64	0.000E 00	0.000E 00	0.000E 00	0.151E-03	0.474E-02
	65	0.000E 00	0.000E 00	0.000E 00	0.107E-03	0.388E-02
	66	0.000E 00	0.000E 00	0.000E 00	0.000E 00	0.317E-02
	67	0.000E 00	0.000E 00	0.000E 00	0.000E 00	0.2576-02
	68	0.000E 00	0.000E 00	0.000E 00	0.000E 00	0.207E-02
	69	0.000E 00	0.000E 00	0.000E 00	0.000E 00	0.167E-02
	70	0.000E 00	0.000E 00	0.000E 00	0.000E 00	0.133E-02
	71	0.000E 00	0.000E 00	0.000E 00	0.000E 00	0.106E-02
	72	0.000E 00	0.000E 00	0.000E 00	0.000E 00	0.845E-03
	73	0.000E 00	0.000E 00	0.000F 00	0.000F 00	0.668E-03
	74	0.000E 00	0.000F 00	0.000F 00	0.000F 00	0-525F-03
	75	0.000F 00	0.000E 00	0.0005 00	0.000F 00	0.4115-03
	76	0.000E 00	0.000E 00	0.0005 00	0.0005 00	0-3205-03
	77	0.000F 00	0.000F 00	0.000F 00	0.0005 00	0.2485-03
	78	0.000E 00	0.000E 00	0.000E 00	0.000E 00	0.1925-03
	79	0.000E 00	0.000E 00	0.000E 00	0.000F 00	0.1475-03
	80	0.000E 00	0.000E 00	0.000E 00	0.000E 00	0.113E-03
	81	0.000E 00	0.000E 00	0.000E 00	0.000F 00	0.000F 00
	82	0.000E 00	0.000E 00	0.000E 00	0.000E 00	0.000E 00
	83	0.000E 00	0.000E 00	0.000E 00	0.000F 00	0.000F 00
	84	0.000E 00	0.000E 00	0.000E 00	0.0005 00	0.0005 00
	85	0.000F 00	0.0005 00	0.0005 00	0.0000 00	0.0005 00
	86	0.000E 00	0.000E 00	0.000E 00	0.000F 00	0.000E 00
	87	0.000F 00	0.000F 00	0.0005 00	0.0005 00	0.000F 00
	88	0.000F 00	0.000F 00	0.0005 00	0.0005 00	0.000E 00
	89	0.0005 00	0.0005 00	0.0005 00	0.0005 00	0-0005 00
	90	0.000E 00	0.000E 00	0.0005 00	0.0005 00	0.0005 00
	91	0.0005 00	0.0005 00	0.0000 00	0.0006 00	0.0006.00
	02	0.0005 00	0.0005 00	0.0005 00	0.0005 00	
	62	0.0005 00	0.0005 00	0.0005 00	0.0000 00	0.0000 00
	40	0.0000 00	0.0000 00	0.0000 00	0.0000 00	0.0000 00
	05	0.0000 00	0.00000 00	0.0000 00	0.0002 00	0.0005 00
	04	0.0000 00	0.0000 00		0.0000 00	0.0000 00
	07	0.0000 00	0.0000 00		0.0002 00	0.0005 00
	200		0.0000 00	0.0002 00	0.0002 00	
	90	0.0000 00	0.0002 00	0.0000 00		0.0000 00
	33	0.0000 00	0.0002 00	0.0002 00	0.0000 00	0.0002 00
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TYPE OF ATOM IS CS MASS= 0.22080E-21GRAMS TEMPERATURE= 450.0DEG. K.

ACCORDING TO MAXWELLIAN DISTRIBUTION, VMP=(2KT/M)**.5, AV=(8KT/3.141M)**.5, RMSV=(3KT/M)**.5

VMP= 0.23720E 05CM/SEC AV= 0.26768E 05CM/SEC RMSV= 0.29051E 05CM/SEC

ACCORDING TO EFFUSIVE FLOW DISTRIBUTION, VMP=(3KT/M)**.5, AV=.75(2*3.141KT/M)**.5, RMSV=(KT/M)**.5

VMP= 0.29051E 05CM/SEC AV= 0.31529E 05CM/SEC RMSV= 0.16772E 05CM/SEC

TIME= 0.172E-02SEC DISTANCE= 0.500E 02CM FOR POINTS 1

TIME= 0.344E-02SEC DISTANCE= 0.100E 03CM FOR POINTS 2

TIME= 0.516E-02SEC DISTANCE= 0.150E 03CM FOR POINTS 3

a

TIME= 0.688E-02SEC DISTANCE= 0.200E 03CM FOR POINTS 4

TIME= 0.860E-02SEC DISTANCE= 0.250E 03CM FOR POINTS 5

PLOT OF I VS S ACCORDING TO THE EQUATION I=C(S**3/T**4)*E**(-BS**2/T**2)

INCREM	ENT ALONG X-AXIS=	9.0CM 0	ONSTANT TIME	UNNORMALIZED	DATA		
 STEP	DISTANCE(IN CM)	POINTS 1	POINTS 2	POINTS 3	POINTS 4	POINTS 5	
1	0.0	0.000E 00	0.000E 00	0.000E 00	0.000E 00	0.000E 00	
2	9.0	0.791E 14	0.513E 13	0.102E 13	0.323E 12	0.1326 12	
3	18.0	0.547E 15	0.395E 14	0.803E 13	0.2568 13	0.105E 13	
4	27.0	0.144E 16	0.125E 15	0.263E 14	0.852E 13	0.352E 13	
5	36.0	0.244E 16	0.273E 15	0.602E 14	0.197E 14	0.824E 13	
 6	45.0	0.308E 16	0.479E 15	0.112E 15	0.376E 14	0.158E 14	
7	54.0	0.311E 16	0.724E 15	0.182E 15	0.628E 14	0.267E 14	
8	63.0	0.263E 16	0.982E 15	0.270E 15	0.959E 14	0.414E 14	
9	72.0	0.189E 16	0.122E 16	0.371E 15	0.136E 15	0.601E 14	
10	81.0	0.118E 16	0.141E 16	0.482E 15	0.1848 15	0.827E 14	1
11	90.0	0.643E 15	0.154E 16	0.597E 15	0.239E 15	0.109E 15	
12	99.0	0.308E 15	0.158E 16	0.710E 15	0.299E 15	0.139E 15	
13	108.0	0.131E 15	0.155E 16	0.814E 15	0.362E 15	0.173E 15	
14	117.0	0.494E 14	0.146E 16	0.904E 15	0.426E 15	0.210E 15	
15	126.0	0.166E 14	0.131E 16	0.976E 15	0.491E 15	0.249E 15	
16	135.0	0.499E 13	0.113E 16	0.102E 16	0.553E 15	0.289E 15	
17	144.0	0.134E 13	0.948E 15	0.105E 16	0.610E 15	0.331E 15	
18	153.0	0.3248 12	0.761E 15	0.105E 16	0.662E 15	0.372E 15	
19	162.0	0.702E 11	0.590E 15	0.103E 16	0.707E 15	0.412E 15	
20	171.0	0.136E 11	0.443E 15	0.100E 16	0.7438 15	0.451E 15	
21	180.0	0.239E 10	0.321E 15	0.946E 15	0.770E 15	0.488E 15	
22	189.0	0.378E 09	0.226E 15	0.877E 15	0.7876 15	0.522E 15	
23	198.0	0.538E 08	0.154E 15	0.800E 15	0.794E 15	0.552E 15	
24	207.0	0.690E 07	0.102E 15	0.717E 15	0.791E 15	0.578E 15	
 25	216.0	0.799E 06	0.655E 14	0.6328 15	0.779E 15	0.599E 15	
26	225.0	0.834E 05	0.408E 14	0.548E 15	0.759E 15	0.6168 15	
27	234.0	0.787E 04	0.247E 14	0.468E 15	0.731E 15	0.627E 15	

	20	242 0	0 (715 0)	0 1/00 1/	0 2020 10			
(	20	243.0	0.6716 03	0.0216 12	0.3936 15	0.697E 15	0.6345 15	
	29	252.0	0.5162 02	0.831E 13	0.3266 15	0.658E 15	0.6355 15	
	30	201.0	0.359E 01	0.4625 13	0.2005 15	0.615E 15	0.632E 15	
	31	270.0	0.2262 00	0.2498 13	0.2148 15	0.5698 15	0.6232 15	
(	32	279.0	0.128E-01	0.131E 13	0.170E 15	0.5218 15	0.611E 15	
	33	288.0	0.6636-03	0.6728 12	0.133E 15	0.474E 15	0.595E 15	
		297.0	0.308E-04	0.334E 12	0.1028 15	0.426E 15	0.575E 15	
	55	306.0	0.130E-05	0.162E 12	0.784E 14	0.380E 15	0.552E 15	
	36	315.0	0.496E-07	0.765E 11	0.589E 14	0.336E 15	0.526E 15	
	37	324.0	0.171E-08	0.351E 11	0.437E 14	0.2958 15	0.499E 15	
(	38	333.0	0.535E-10	0.157E 11	0.319E 14	0.257E 15	0.470E 15	
	39	342.0	0.151E-11	0.684E 10	0.231E 14	0.221E 15	0.440E 15	
	40	351.0	0.388E-13	0.290E 10	0.164E 14	0.189E 15	0.409E 15	
	41	360.0	0.901E-15	0.1198 10	0.116E 14	0.160E 15	0.379E 15	
-	42	369.0	0.189E-16	0.482E 09	0.807E 13	0.135E 15	0.348E 15	
	43	378.0	0.360E-18	0.189E 09	0.554E 13	0.113E 15	0.319E 15	
	he he	387.0	0.000E 00	0.7238 08	0.376E 13	0.938E 14	0.290E 15	
	45	396.0	0.000E 00	0.269E 08	0.2518 13	0.772E 14	0.262E 15	
	46	405.0	0.000E 00	0-976E 07	0.166E 13	0.630E 14	0-236F 15	
( ·	47	414.0	0.000E 00	0.345F 07	0.108E 13	0.510F 14	0.2116 15	
	48	423.0	0.0005 00	0.118F 07	0.702E 12	0.410F 14	0.1885 15	
	40	432.0	0.0005 00	0.3095 06	0.4485 12	0.3276 14	0.1665 15	
	50	441.0	0.0005 00	0 1305 06	0.2026 12	0 2505 14	0 1446 15	
( · · · · · · · · · · · · · · · · · · ·	51	450.0	0.0005.00	0.4176.05	0 1755 12	0 2046 14	0 1295 15	
	ン <u>↓</u> につ	450.0	0.0002 00	0 1205 05	0 1005 12	0 1606 14	0.1200 10	
	26	439.0	0.0002 00	0.1296 05	0.1086 12	0.1096 14	0.0745 14	
C 2	23	400.0	0.0002 00	0.3936 04	0.6576 11	0.1235 14	0.9/45 14	
	24	4/1.0	0.0000 00	0.116E 04	0.394E 11	0.9518 13	0.8412 14	
	22	486.0	0.0002 00	0.3358 03	0.2348 11	0.727E 13	0.722E 14	
	56	492.0	0.0000 00	0.943E 02	0.137E 11	0.551E 13	0.617E 14	é
C	57	504.0	0.000E 00	0.258E 02	0.796E 10	0.415E 13	0.525E 14	
	58	513.0	0.000E 00	0.690E 01	0.456E 10	0.311E 13	0.444E 14	
	59	522.0	0.000E 00	0.179E 01	0.258E 10	0.231E 13	0.374E 14	
	60	531.0	0.000E 00	0.4568 00	0.144E 10	0.170E 13	0.314E 14	
	61	540.0	0.000E 00	0.113E 00	0.799E 09	0.124E 13	0.262E 14	
L	62	549.0	0.000E 00	0.273E-01	0.437E 09	0.909E 12	0.217E 14	
	63	558.0	0.000E 00	0.644E-02	0.236E 09	0.657E 12	0.180E 14	
· · · · · · · · · · · · · · · · · · ·	64	567.0	0.000E 00	0.148E-02	0.126E 09	0.4718 12	0.148E 14	
	65	576.0	0.000E 00	0.331E-03	0.666E 08	0.336E 12	0.121E 14	
	66	585.0	0.000E 00	0.724E-04	0.347E 08	0.237E 12	0.989E 13	
	67	594.0	0.000E 00	0.154E-04	0.1796 08	0.167E 12	0.802E 13	
	68	603.0	0.000E 00	0.3216-05	0.915E 07	0.116E 12	0.648E 13	
	69	612.0	0.000E 00	0.650E-06	0.4618 07	0.8108 11	0.5216 13	
	70	621.0	0.000E 00	0.128E-06	0.230E 07	0.558E 11	0.417E 13	
	71	630.0	0.000E 00	0.248E-07	0.113E 07	0.382E 11	0.332E 13	
	72	639.0	0.000E 00	0.467E-08	0.5528 06	0.260E 11	0.263E 13	
	73	648.0	0.000F 00	0-857E-09	0.266F 06	0.175E 11	0.208E 13	
	74	657.0	0.000F 00	0-153E-09	0.126E 06	0.1176 11	0.1635 13	
	75	666.0	0.000F 00	0.267E-10	0.597E 05	0.7855 10	0.1285 13	
	76	675.0	0.000F 00	0.4565-11	0.2786 05	0.520E 10	0.9995 12	
	77	684.0	0.0005 00	0.7586-12	0.1285 05	0.3425 10	0.7756 12	
	78	693.0	0.0005 00	0.1226-12	0.6835 04	0.2225 10	0.5005 12	
	70	702.0	0.0005 00	0.1046-12	0 2626 04	0 1455 10	0 6405 12	
	àn	711 0	0.0000 00	0 2005-14	0 1145 04	0 0255 00	0.96000 12	
< · · ·		720.0	0.0005 00	0 4505-15	0 5145 03	0.5005.00	0.3265 12	
	01	720.0	0.0002 00	0.4506-15	0.2296 03	0.3475 04	0.2686 12	
	62	729.0	0.0000 00	0.001E-10	0.223E 03	0.3818 09	0.204E 12	
	83	138.0	0.000E 00	0.94/E-1/	0.9628 02	0.241E 09	0.1946 12	
	84	141.0	0.000E 00	0.1328-17	0.409E 02	0.151E 09	0.116E 12	
	85	156.0	0.000E 00	0.180E-18	0.172E 02	0.946E 08	0.869E 11	
	86	165.0	0.000E 00	0.239E-19	0.716E 01	0.586E 08	0.6488 11	
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6	88	783.0	0.000E 00	0.000E 00	0.119E 01	0.2216 08	0.356E 11	
C .	90	801.0	0.000E 00	0.000E 00	0.4826 00	0.1348 08	0.1925 11	
_	91	810.0	0.000E 00	0.000E 00	0.7546-01	0.488E 07	0.140E 11	
Ć	92	819.0	0.000E 00	0.000E 00	0.293E-01	0.2916 07	0.1026 11	
	93	828.0	0.000E 00	0.000E 00	0.112E-01	0.172E 07	0.739E 10	
6-	94	845.0	0.000E 00	0.000E 00	0.4295-02	0.101E 07	0.5332 10	
	96	855.0	0.000E 00	0.000E 00	0.600E-03	0.3455 06	0.2735 10	
	97	864.0	0.000E 00	0.000E 00	0.2216-03	0.199E 06	0.194E 10	
( -	98	873.0	0.000E 00	0.000E 00	0.804E-04	0.114E 06	0.138E 10	
	99	882.0	0.000E 00	0.000E 00	0.2895-04	0.654E 05	0.974E 09	
C .	100	091.0	0.0002 00	0.0000 00	0.1026-04	0.3708 05	0.0855 04	
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DATA FOR PLOTS           STEP         POINTS 1         POINTS 2         POINTS 3         POINTS 4         POINTS 5           1         0.00000 00         0.00000 00         0.00000 00         0.00000 00           1         0.00000 00         0.00000 00         0.00000 00         0.00000 00           1         0.00000 00         0.00000 00         0.00000 00         0.00000 00           1         0.00000 00         0.00000 00         0.00000 00         0.00000 00           1         0.00000 00         0.00000 00         0.00000 00         0.00000 00           1         0.00000 00         0.00000 00         0.00000 00         0.00000 00           1         0.000000 00         0.00000 00         0.00000 00         0.00000 00         0.0000000           1         0.000000 00         0.00000 00         0.00000 00         0.00000000000000000000000000000000000	RANGE =	0.100E 01 VALUE OF A	TOP =	0.100E 01 00E 00	BOTTOM =	0.000E 00	SCALE = 0.100E-01 PER STEP	
STEP         POINTS 1         POINTS 2         POINTS 3         POINTS 4         POINTS 5           1         0.00000000000000000000000000000000000	DATA FOR	RPLOTS		519192009 - 1309493				
1100       PULKES 1       PULKES 3       PULKES 3         1       0.0000       0.1000       0.0000       0.0000         2       0.2534-01       0.1044-02       0.2274-03       0.0000       0.0000         3       0.1755       0.0000       0.2774-02       0.1234-03       0.0000       0.0000         4       0.4440       0.4440-03       0.2774-02       0.1234-03       0.1334-03         4       0.4440       0.4440-03       0.1340-01       0.5347-03       0.1334-01         4       0.44440       0.1314       0.0007-01       0.5347-01       0.5347-01         4       0.44440       0.0114       0.0007-01       0.5347-01       0.1372-01         5       0.44440       0.0114       0.000       0.4772-01       0.3357-01         11       0.45440       0.0114       0.0000       0.4772-01       0.3357-01         11       0.45450       0.0000       0.2772-00       0.4984-01       0.4440-01         12       0.45450       0.0000       0.2772-00       0.4984-01       0.4440-01         13       0.4545-01       0.4440-00       0.3272-01       0.4596-01       0.4440-01         14       0.4545-01 <t< td=""><td>C 17 C D</td><td>DOTNEC 1</td><td>OOTHTO O</td><td>and the state of the</td><td>001100</td><td></td><td></td><td></td></t<>	C 17 C D	DOTNEC 1	OOTHTO O	and the state of the	001100			
$\begin{array}{c} 1 & 0.4000 & 00 & 0.4000 & 00 & 0.4000 & 00 & $	SIEP	PUINIS	PUINIS 2	PUINIS 3	PUINIS 4	PUINTS 5		
2       0.233-01       0.144-02       0.3776-03       0.0000         4       0.4440       0.4420-01       0.43776-03       0.1386-02         5       0.1576-00       0.13776-03       0.1386-02       0.4466-02         6       0.43776-03       0.1387-03       0.4386-02       0.4466-02         7       0.1000-01       0.2326-00       0.5666-01       0.2016-01       0.4386-02         9       0.4647-00       0.3316-00       0.4386-01       0.4386-01       0.4386-01         10       0.3786-00       0.4386-01       0.4386-01       0.4386-01       0.4386-01         11       0.4366-01       0.4386-01       0.4386-01       0.4386-01       0.4386-01         11       0.4386-01       0.44680       0.4386-01       0.4386-01       0.4386-01         12       0.4386-01       0.44680       0.33860       0.4386-01       0.4386-01         13       0.4386-01       0.44690       0.33860       0.4386-01       0.4386-01         14       0.1386-00       0.43860       0.4386-01       0.4386-01       0.4386-01         14       0.1386-00       0.33860       0.4386-01       0.4386-01       0.4386-01         14       0.13860	1	0.000E 00	0.000E 00	0.000E 00	0.000E 00	0.000E 00		
$\begin{array}{c} 3 & 0 & 175 & 00 & 0.126 & -01 & 0.237 & -0.2 & 0.222 & -0.3 & 0.336 & -03 \\ \hline & 0 & 0.47 & -00 & 0.137 & -01 & 0.137 & -01 & 0.634 & -02 & 0.264 & -02 \\ \hline & 0 & 0.47 & 01 & 0.137 & -01 & 0.634 & -02 & 0.264 & -02 \\ \hline & 0 & 0.47 & 01 & 0.137 & -01 & 0.634 & -02 & 0.264 & -02 \\ \hline & 0 & 0.47 & 01 & 0.137 & -01 & 0.634 & -02 & 0.264 & -02 \\ \hline & 0 & 0.47 & 01 & 0.137 & -01 & 0.634 & -02 & 0.264 & -02 \\ \hline & 0 & 0.47 & 01 & 0.137 & -01 & 0.634 & -02 & 0.264 & -02 \\ \hline & 0 & 0.47 & 00 & 0.334 & 00 & 0.664 & -01 & 0.477 & -01 & 0.1372 & -01 \\ \hline & 0 & 0.474 & 00 & 0.431 & 00 & 0.154 & 00 & 0.572 & -01 & 0.636 & -01 \\ \hline & 10 & 0.474 & 00 & 0.443 & 00 & 0.154 & 00 & 0.572 & -01 & 0.636 & -01 \\ \hline & 11 & 0.706 & 00 & 0.473 & 00 & 0.2274 & 00 & 0.956 & -01 & 0.4446 & -01 \\ \hline & 12 & 0.4907 & -01 & 0.594 & 00 & 0.2274 & 00 & 0.956 & -01 & 0.4446 & -01 \\ \hline & 13 & 0.4307 & -03 & 0.305 & 00 & 0.3376 & 00 & 0.1776 & 00 & 0.9766 & -01 \\ \hline & 14 & 0.106 & -02 & 0.3424 & 00 & 0.3376 & 00 & 0.1776 & 00 & 0.9766 & -01 \\ \hline & 14 & 0.4307 & -03 & 0.305 & 00 & 0.3376 & 00 & 0.1776 & 00 & 0.9766 & -01 \\ \hline & 14 & 0.4307 & -03 & 0.305 & 00 & 0.3376 & 00 & 0.1262 & 00 & 0.1066 & 0 \\ \hline & 12 & 0.0007 & 00 & 0.1426 & 00 & 0.3376 & 00 & 0.1262 & 00 & 0.1066 & 0 \\ \hline & 22 & 0.0007 & 00 & 0.1426 & 00 & 0.3376 & 00 & 0.2756 & 00 & 0.1776 & 00 \\ \hline & 22 & 0.0007 & 00 & 0.3776 & -01 & 0.2766 & 00 & 0.1576 & 00 \\ \hline & 22 & 0.0007 & 00 & 0.3776 & -01 & 0.2766 & 00 & 0.2786 & 00 & 0.1776 & 00 \\ \hline & 22 & 0.0007 & 00 & 0.1776 & 00 & 0.2786 & 00 & 0.1776 & 00 \\ \hline & 23 & 0.0007 & 00 & 0.1066 & 0 & 0.1266 & 00 & 0.2786 & 00 & 0.1976 & 00 \\ \hline & 33 & 0.0007 & 00 & 0.12770 & 0.2786 & 00 & 0.1776 & 00 \\ \hline & 34 & 0.0007 & 00 & 0.12770 & 0.12786 & 00 & 0.2786 & 00 \\ \hline & 34 & 0.0007 & 00 & 0.1276 & 0 & 0.2786 & 00 & 0.1976 & 00 \\ \hline & 34 & 0.0007 & 00 & 0.1266 & 00 & 0.2786 & 00 & 0.1976 & 00 \\ \hline & 33 & 0.0007 & 00 & 0.2566 & -0 & 0.1776 & 00 & 0.2786 & 00 \\ \hline & 34 & 0.0007 & 00 & 0.2606 & 0 & 0.2786 & -0 & 0.1776 & 00 \\ \hline & 34 & 0.0007 & 00 & 0.2606 & 0 & 0.2786 & $	2	0.2538-01	0.164E-02	0.3276-03	0.1038-03	0.000E 00		
$\begin{array}{c} \begin{array}{c} + \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\$	. 3	0.175E 00	0.126E-01	0.257E-02	0.822E-03	0.338E-03		
$\begin{array}{c} 3 & 0.735 \pm 00 & 0.4775 - 01 & 0.1935 - 01 & 0.6345 - 02 & 0.2645 - 02 \\ \hline 0 & 0.975 \pm 00 & 0.535 \pm 00 & 0.536 \pm 01 & 0.2015 - 01 & 0.595 - 02 \\ \hline 1 & 0.1005 \pm 01 & 0.535 \pm 00 & 0.536 \pm 01 & 0.2015 - 01 & 0.595 - 01 \\ \hline 1 & 0.205 \pm 00 & 0.535 \pm 00 & 0.154 \pm 00 & 0.575 \pm -01 & 0.255 - 01 \\ \hline 1 & 0.205 \pm 00 & 0.595 \pm 00 & 0.154 \pm 00 & 0.575 \pm -01 & 0.255 - 01 \\ \hline 1 & 0.205 \pm 00 & 0.595 \pm 00 & 0.154 \pm 00 & 0.575 \pm -01 & 0.255 - 01 \\ \hline 1 & 0.205 \pm 00 & 0.595 \pm 00 & 0.154 \pm 00 & 0.555 \pm -01 & 0.555 \pm -01 \\ \hline 1 & 0.155 \pm -01 & 0.595 \pm 00 & 0.237 \pm 00 & 0.555 \pm -01 & 0.555 \pm -01 \\ \hline 1 & 0.155 \pm -01 & 0.595 \pm 00 & 0.237 \pm 00 & 0.555 \pm -01 & 0.555 \pm -01 \\ \hline 1 & 0.155 \pm -01 & 0.595 \pm 00 & 0.237 \pm 00 & 0.155 \pm 00 & 0.675 \pm -01 \\ \hline 1 & 0.155 \pm -01 & 0.595 \pm 00 & 0.237 \pm 00 & 0.155 \pm 00 & 0.155 \pm 00 \\ \hline 1 & 0.155 \pm -01 & 0.595 \pm 00 & 0.237 \pm 00 & 0.155 \pm 00 & 0.105 \pm 00 \\ \hline 1 & 0.435 \pm -30 & 0.235 \pm 00 & 0.337 \pm 00 & 0.155 \pm 00 & 0.105 \pm 00 \\ \hline 1 & 0.001 \pm 00 & 0.145 \pm 00 & 0.337 \pm 00 & 0.226 \pm 00 & 0.137 \pm 00 \\ \hline 2 & 0.0001 \pm 00 & 0.145 \pm 00 & 0.238 \pm 00 & 0.144 \pm 00 \\ \hline 2 & 0.0001 \pm 00 & 0.135 \pm 00 & 0.238 \pm 00 & 0.145 \pm 00 \\ \hline 2 & 0.0001 \pm 00 & 0.135 \pm 01 & 0.237 \pm 00 & 0.144 \pm 00 \\ \hline 2 & 0.0001 \pm 00 & 0.135 \pm 01 & 0.237 \pm 00 & 0.145 \pm 00 \\ \hline 2 & 0.0001 \pm 00 & 0.135 \pm 01 & 0.237 \pm 00 & 0.238 \pm 00 & 0.147 \pm 00 \\ \hline 2 & 0.0001 \pm 00 & 0.135 \pm 01 & 0.155 \pm 00 & 0.155 \pm 00 \\ \hline 2 & 0.0001 \pm 00 & 0.135 \pm 01 & 0.237 \pm 00 & 0.234 \pm 00 & 0.234 \pm 00 \\ \hline 2 & 0.0001 \pm 00 & 0.135 \pm 01 & 0.155 \pm 00 & 0.157 \pm 00 \\ \hline 2 & 0.0001 \pm 00 & 0.135 \pm 01 & 0.155 \pm 00 & 0.157 \pm 00 \\ \hline 2 & 0.0001 \pm 00 & 0.135 \pm 01 & 0.167 \pm 00 & 0.234 \pm 00 & 0.205 \pm 00 \\ \hline 3 & 0.0001 \pm 00 & 0.135 \pm 01 & 0.167 \pm 00 & 0.234 \pm 00 & 0.205 \pm 00 \\ \hline 3 & 0.0001 \pm 00 & 0.0005 \pm 00 & 0.134 \pm 00 & 0.234 \pm 00 & 0.234 \pm 00 \\ \hline 3 & 0.0001 \pm 00 & 0.0005 \pm 00 & 0.134 \pm 00 & 0.234 \pm 00 \\ \hline 3 & 0.0001 \pm 00 & 0.0005 \pm 00 & 0.135 \pm 00 & 0.158 \pm 00 \\ \hline 3 & 0.0001 \pm 00 & 0.0005 \pm 00 & 0.135 \pm 00 & 0.158 \pm 00 \\ \hline 3 & 0.00001 \pm 00 & 0.0005 \pm 00 & 0.234 \pm 00 & 0.158 \pm 00 \\ \hline 3 & 0.0$	4	0.464E 00	0.402E-01	0.845E-02	0.273E-02	0.113E-02		
6       0.9876 00       0.1358 00       0.3596-01       0.1205-01       0.5876-02         7       0.1006 01       0.2328 00       0.6856-01       0.3076-01       0.3326-01         9       0.6846 00       0.3146 00       0.6856-01       0.3076-01       0.3265-01         10       0.7976 00       0.4936 00       0.4146 00       0.4646-01       0.3076-01         11       0.2066 00       0.4936 00       0.2116 00       0.7676-01       0.3306-01         13       0.4206-01       0.5006 00       0.2216 00       0.4646-01       0.3366-00         13       0.4206-01       0.5006 00       0.2216 00       0.1646 00       0.5566-01         14       0.1536-00       0.6738-01       0.4646 00       0.5376-01         14       0.1536 00       0.2346 00       0.1376 00       0.2346 00       0.1376 00         14       0.4376 00       0.3376 00       0.2346 00       0.1376 00       0.2346 00         14       0.4376 00       0.3376 00       0.2346 00       0.1476 00       0.2346 00         15       0.0006 00       0.1427 00       0.2346 00       0.1476 00       0.2346 00         15       0.0006 00       0.2376 00       0.2346 00       0.1476		0.783E 00	0.877E-01	0.193E-01	0.634E-02	0.264E-02		7,8%
$\begin{array}{c} 7 \\ 0 & 0.100 \\ 0 & 0.232 \\ 0 & 0.232 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.231 \\ 0 & 0.2$	6	0.987E 00	0.153E 00	0.3596-01	0.120E-01	0.5078-02		
$ \begin{array}{c} 8 \\ 0 & 0.4944 \\ 0 & 0 & 0.3444 \\ 0 & 0 & 0.3444 \\ 0 & 0 & 0.4344 \\ 0 & 0 & 0.4344 \\ 0 & 0 & 0 & 0.4344 \\ 0 & 0.5344 \\ 0 & 0 & 0.4344 \\ 0 & 0.5344 \\ 0 & 0 & 0.4344 \\ 0 & 0.5344 \\ 0 & 0 & 0.4344 \\ 0 & 0.5344 \\ 0 & 0 & 0.4344 \\ 0 & 0.5344 \\ 0 & 0.4204 \\ 0 & 0 & 0.4044 \\ 0 & 0.4204 \\ 0 & 0 & 0.4044 \\ 0 & 0.4204 \\ 0 & 0 & 0.4044 \\ 0 & 0.4204 \\ 0 & 0 & 0.4044 \\ 0 & 0.4204 \\ 0 & 0 & 0.4044 \\ 0 & 0.4204 \\ 0 & 0 & 0.4044 \\ 0 & 0.4204 \\ 0 & 0 & 0.4044 \\ 0 & 0.4204 \\ 0 & 0 & 0.4044 \\ 0 & 0.4204 \\ 0 & 0 & 0.4044 \\ 0 & 0.4204 \\ 0 & 0 & 0.4044 \\ 0 & 0.4204 \\ 0 & 0 & 0.4044 \\ 0 & 0.4204 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ 0 & 0.4044 \\ $	7	0.1008 01	0.232E 00	0.584E-01	0.201E-01	0.858E-02		
$\begin{array}{c} 9 & 0.4076 & 00 & 0.3916 & 00 & 0.196 & 00 & 0.4386 & 01 & 0.5926 & 01 \\ 10 & 0.5966 & 01 & 0.4356 & 00 & 0.5926 & 01 & 0.2926 & 01 \\ 11 & 0.5966 & 01 & 0.4356 & 00 & 0.5926 & 01 & 0.2556 & 01 \\ 12 & 0.5966 & 01 & 0.4056 & 00 & 0.2816 & 00 & 0.1166 & 01 & 0.5566 & 01 \\ 13 & 0.4206 & 01 & 0.4056 & 00 & 0.2816 & 00 & 0.1166 & 01 & 0.5566 & 01 \\ 14 & 0.1586 & 01 & 0.4056 & 00 & 0.2896 & 00 & 0.1576 & 00 & 0.5796 & 01 \\ 15 & 0.5336 & 02 & 0.3366 & 00 & 0.3376 & 00 & 0.1576 & 00 & 0.5796 & 01 \\ 15 & 0.5336 & 02 & 0.3376 & 00 & 0.1576 & 00 & 0.5268 & 01 \\ 14 & 0.1036 & 03 & 0.0386 & 00 & 0.2266 & 00 & 0.1956 & 00 & 0.1066 & 00 \\ 15 & 0.0006 & 00 & 0.1486 & 00 & 0.2266 & 00 & 0.1956 & 00 & 0.1066 & 00 \\ 15 & 0.0006 & 00 & 0.1486 & 00 & 0.2266 & 00 & 0.1486 & 00 \\ 24 & 0.0006 & 00 & 0.1486 & 00 & 0.2266 & 00 & 0.1476 & 00 \\ 24 & 0.0006 & 00 & 0.2756 & 01 & 0.2266 & 00 & 0.1776 & 00 \\ 25 & 0.0006 & 00 & 0.2756 & 01 & 0.2266 & 00 & 0.1776 & 00 \\ 25 & 0.0006 & 00 & 0.2276 & 00 & 0.2266 & 00 & 0.1976 & 00 \\ 26 & 0.0006 & 00 & 0.2726 & 00 & 0.2266 & 00 & 0.1976 & 00 \\ 26 & 0.0006 & 00 & 0.2266 & 00 & 0.2266 & 00 & 0.1976 & 00 \\ 26 & 0.0006 & 00 & 0.2266 & 00 & 0.2266 & 00 & 0.1976 & 00 \\ 26 & 0.0006 & 00 & 0.2266 & 00 & 0.2266 & 00 & 0.1976 & 00 \\ 26 & 0.0006 & 00 & 0.2266 & 00 & 0.2266 & 00 & 0.1976 & 00 \\ 27 & 0.0006 & 00 & 0.2266 & 00 & 0.2266 & 00 & 0.1976 & 00 \\ 28 & 0.0006 & 00 & 0.2266 & 00 & 0.2266 & 00 & 0.1976 & 00 \\ 29 & 0.0006 & 00 & 0.2266 & 00 & 0.2266 & 00 & 0.1976 & 00 \\ 31 & 0.0006 & 00 & 0.2266 & 00 & 0.2266 & 00 & 0.1976 & 00 \\ 32 & 0.0006 & 00 & 0.2266 & 00 & 0.2266 & 00 & 0.1976 & 00 \\ 33 & 0.0006 & 00 & 0.2266 & 00 & 0.2266 & 00 & 0.1976 & 00 \\ 33 & 0.0006 & 00 & 0.2266 & 00 & 0.2266 & 00 & 0.1976 & 00 \\ 33 & 0.0006 & 00 & 0.2266 & 00 & 0.2266 & 00 & 0.1976 & 00 \\ 33 & 0.0006 & 00 & 0.0006 & 00 & 0.2266 & 00 & 0.1976 & 00 \\ 33 & 0.0006 & 00 & 0.0006 & 00 & 0.2266 & 00 & 0.1976 & 00 \\ 34 & 0.0006 & 00 & 0.0006 & 00 & 0.2266 & 00 & 0.1976 & 00 \\ 34 & 0.0006 & 00 & 0.0006 & 00 & 0.2266 & 00 & 0.196$	8	0.844E 00	0.314E 00	0.865E-01	0.307E-01	0.1328-01		
$ \begin{array}{c} 10 & 0.776 & 00 & 0.7376 & 00 & 0.7376 & 00 & 0.7776 & 00 & 0.3507 & -01 \\ 11 & 0.7906 & 00 & 0.7916 & 00 & 0.7776 & 00 & 0.3507 & -01 \\ 12 & 0.7906 & 00 & 0.7916 & 00 & 0.7776 & 00 & 0.3507 & -01 \\ 13 & 0.73316 & -02 & 0.7426 & 00 & 0.3286 & 00 & 0.3786 & -01 \\ 14 & 0.73316 & -02 & 0.7426 & 00 & 0.3286 & 00 & 0.7786 & 00 & 0.7926 & -01 \\ 15 & 0.73316 & -02 & 0.7306 & 00 & 0.3786 & 00 & 0.7786 & 00 & 0.7926 & -01 \\ 16 & 0.7108 & -03 & 0.3036 & 00 & 0.3376 & 00 & 0.7286 & 00 & 0.1046 & 00 \\ 19 & 0.0006 & 00 & 0.1426 & 00 & 0.2316 & 00 & 0.2326 & 00 & 0.1196 & 00 \\ 19 & 0.0006 & 00 & 0.1426 & 00 & 0.2316 & 00 & 0.2326 & 00 & 0.1276 & 00 \\ 20 & 0.0006 & 00 & 0.1226 & 00 & 0.2316 & 00 & 0.2326 & 00 & 0.1446 & 00 \\ 21 & 0.0006 & 00 & 0.1226 & 00 & 0.2326 & 00 & 0.1276 & 00 \\ 22 & 0.0006 & 00 & 0.2376 & 01 & 0.2296 & 00 & 0.1676 & 00 \\ 23 & 0.0006 & 00 & 0.2376 & 01 & 0.2296 & 00 & 0.1776 & 00 \\ 24 & 0.0006 & 00 & 0.2376 & 01 & 0.2296 & 00 & 0.1276 & 00 \\ 24 & 0.0006 & 00 & 0.2376 & 01 & 0.2386 & 00 & 0.2396 & 00 \\ 24 & 0.0006 & 00 & 0.7266 & 0.2716 & 00 & 0.2346 & 00 & 0.2376 & 00 \\ 24 & 0.0006 & 00 & 0.7266 & 0.2716 & 00 & 0.2346 & 00 & 0.2016 & 00 \\ 24 & 0.0006 & 00 & 0.7266 & -0.1196 & 00 & 0.2234 & 00 & 0.2016 & 00 \\ 24 & 0.0006 & 00 & 0.7266 & -0.1196 & 00 & 0.2234 & 00 & 0.2016 & 00 \\ 24 & 0.0006 & 00 & 0.1466 & -0.0688 & -01 & 0.1776 & 00 & 0.2038 & 00 \\ 31 & 0.0006 & 00 & 0.4266 & -0.1046 & 00 & 0.2346 & 00 & 0.2016 & 00 \\ 33 & 0.0006 & 00 & 0.4266 & -0.0146 & 00 & 0.2346 & 00 & 0.2016 & 00 \\ 33 & 0.0006 & 00 & 0.4266 & -0.0146 & 0.01766 & 0.02006 & 00 \\ 34 & 0.0006 & 00 & 0.4266 & -0.0146 & 00 & 0.2346 & 00 & 0.2038 & 00 \\ 33 & 0.0006 & 00 & 0.4266 & -0.0146 & 00 & 0.2346 & 00 & 0.2038 & 00 \\ 33 & 0.0006 & 00 & 0.4266 & -0.0146 & 00 & 0.2346 & 00 \\ 33 & 0.0006 & 00 & 0.4266 & -0.0146 & 0.0246 & 00 & 0.2006 & 00 \\ 34 & 0.0006 & 00 & 0.0066 & 00 & 0.2346 & 00 & 0.2006 & 00 \\ 34 & 0.0006 & 00 & 0.0066 & 00 & 0.2346 & 00 & 0.2006 & 00 \\ 34 & 0.0006 & 00 & 0.0066 & 00 & 0.2346 & 00 & 0.2006 & 00 \\ 34 & 0$	9	0.607E 00	0.391E 00	0.1198 00	0.438E-01	0.1926-01		
$\begin{array}{c} 11 & 0.708 \pm 00 & 0.793 \pm 00 & 0.791 \pm 00 & 0.791 \pm 00 & 0.791 \pm 00 \\ 13 & 0.720 \pm 00 & 0.791 \pm 00 & 0.791 \pm 00 & 0.791 \pm 00 \\ 14 & 0.791 \pm 00 & 0.791 \pm 00 & 0.791 \pm 00 \\ 15 & 0.731 \pm 00 & 0.791 \pm 00 & 0.791 \pm 00 \\ 15 & 0.731 \pm 00 & 0.791 \pm 00 & 0.791 \pm 00 \\ 16 & 0.100 \pm 00 & 0.791 \pm 00 & 0.791 \pm 00 \\ 17 & 0.791 \pm 00 & 0.791 \pm 00 & 0.791 \pm 00 \\ 18 & 0.103 \pm 03 & 00 & 0.731 \pm 00 & 0.771 \pm 00 & 0.791 \pm 00 \\ 18 & 0.103 \pm 03 & 00 & 0.731 \pm 00 & 0.721 \pm 00 \\ 19 & 0.000 \pm 00 & 0.1481 \pm 00 & 0.7331 \pm 00 & 0.721 \pm 00 \\ 20 & 0.000 \pm 00 & 0.1481 \pm 00 & 0.7331 \pm 00 & 0.731 \pm 00 \\ 21 & 0.000 \pm 00 & 0.1481 \pm 00 & 0.7331 \pm 00 & 0.731 \pm 00 \\ 22 & 0.000 \pm 00 & 0.725 \pm 01 & 0.231 \pm 00 & 0.731 \pm 00 \\ 23 & 0.000 \pm 00 & 0.725 \pm 01 & 0.231 \pm 00 & 0.733 \pm 00 \\ 24 & 0.000 \pm 00 & 0.725 \pm 01 & 0.231 \pm 00 & 0.733 \pm 00 \\ 24 & 0.000 \pm 00 & 0.725 \pm 01 & 0.234 \pm 00 & 0.731 \pm 00 \\ 24 & 0.000 \pm 00 & 0.725 \pm 01 & 0.234 \pm 00 & 0.731 \pm 00 \\ 24 & 0.000 \pm 00 & 0.725 \pm 01 & 0.234 \pm 00 & 0.731 \pm 00 \\ 24 & 0.000 \pm 00 & 0.725 \pm 01 & 0.724 \pm 00 & 0.731 \pm 00 \\ 24 & 0.000 \pm 00 & 0.725 \pm 01 & 0.224 \pm 00 & 0.234 \pm 00 \\ 24 & 0.000 \pm 00 & 0.725 \pm 01 & 0.224 \pm 00 & 0.234 \pm 00 \\ 25 & 0.000 \pm 00 & 0.725 \pm 0.116 \pm 00 & 0.234 \pm 00 \\ 24 & 0.000 \pm 00 & 0.724 \pm 0.0 & 0.234 \pm 00 \\ 25 & 0.000 \pm 00 & 0.64 \pm 0.2 & 0.134 \pm 00 & 0.234 \pm 00 \\ 25 & 0.000 \pm 00 & 0.64 \pm 0.2 & 0.134 \pm 00 & 0.234 \pm 00 \\ 25 & 0.000 \pm 00 & 0.64 \pm 0.2 & 0.134 \pm 00 & 0.234 \pm 00 \\ 25 & 0.000 \pm 00 & 0.64 \pm 0.2 & 0.134 \pm 00 & 0.134 \pm 00 \\ 33 & 0.000 \pm 00 & 0.000 \pm 00 & 0.234 \pm 01 & 0.134 \pm 00 \\ 33 & 0.000 \pm 00 & 0.000 \pm 00 & 0.234 \pm 01 & 0.134 \pm 00 \\ 33 & 0.000 \pm 00 & 0.000 \pm 00 & 0.734 \pm 00 & 0.134 \pm 00 \\ 33 & 0.000 \pm 00 & 0.000 \pm 00 & 0.734 \pm 0.0 & 0.134 \pm 00 \\ 33 & 0.000 \pm 00 & 0.000 \pm 00 & 0.734 \pm 0.0 & 0.134 \pm 00 \\ 34 & 0.000 \pm 00 & 0.000 \pm 00 & 0.734 \pm 0.0 & 0.134 \pm 00 \\ 34 & 0.000 \pm 00 & 0.000 \pm 00 & 0.734 \pm 0.0 & 0.134 \pm 00 \\ 34 & 0.000 \pm 00 & 0.000 \pm 00 & 0.734 \pm 0.0 & 0.134 \pm 00 \\ 34 & 0.000 \pm 00 & 0.000 \pm 00 & 0.734 \pm 0.0 & 0.134 \pm 00 \\ 34 & 0.000 \pm 00 & 0.000 \pm 00 & 0.734 \pm 0.0 & 0.$	10	0.378E 00	0.4538 00	0.154E 00	0.5928-01	0.2652-01		
$\begin{array}{c} 12 & 0.790 \pm 01 & 0.201 & 0.201 & 0.0 & 0.201 & 0.0 & 0.318 \pm 00 & 0.5361 \pm 01 \\ 14 & 0.190 \pm 01 & 0.600 & 00 & 0.201 & 00 & 0.116 \pm 00 & 0.5561 \pm 01 \\ 14 & 0.190 \pm 01 & 0.201 & 0.0 & 0.191 & 00 & 0.1951 & 00 & 0.1971 & 00 \\ 15 & 0.231 \pm 00 & 0.331 \pm 00 & 0.231 \pm 00 & 0.2321 & 00 & 0.1191 & 00 \\ 14 & 0.430 \pm 00 & 0.1421 & 00 & 0.231 \pm 00 & 0.2341 & 00 & 0.2341 & 00 \\ 14 & 0.430 \pm 00 & 0.1421 & 00 & 0.2341 & 00 & 0.2341 & 00 & 0.2341 & 00 \\ 14 & 0.400 \pm 00 & 0.1421 & 00 & 0.2341 & 00 & 0.2341 & 00 & 0.2341 & 00 \\ 22 & 0.400 \pm 00 & 0.1421 & 00 & 0.2341 & 00 & 0.2341 & 00 & 0.2341 & 00 \\ 22 & 0.400 \pm 00 & 0.1421 & 00 & 0.2341 & 00 & 0.2341 & 00 & 0.2341 & 00 \\ 23 & 0.400 \pm 00 & 0.2371 \pm 01 & 0.2341 & 00 & 0.2341 & 00 & 0.2341 & 00 \\ 24 & 0.400 \pm 00 & 0.2371 \pm 01 & 0.2341 & 00 & 0.2341 & 00 & 0.2341 & 00 \\ 25 & 0.400 \pm 00 & 0.2371 \pm 01 & 0.2341 & 00 & 0.2341 & 00 & 0.2341 & 00 \\ 27 & 0.400 \pm 00 & 0.2371 \pm 01 & 0.2341 & 00 & 0.2341 & 00 & 0.1971 & 00 \\ 27 & 0.400 \pm 00 & 0.2371 \pm 01 & 0.2341 & 00 & 0.2341 & 00 & 0.2341 & 00 \\ 27 & 0.400 \pm 00 & 0.23271 \pm 01 & 0.2341 & 00 & 0.2341 & 00 & 0.2341 & 00 \\ 27 & 0.400 \pm 00 & 0.2341 \pm 00 & 0.2341 & 00 & 0.2341 & 00 \\ 28 & 0.400 \pm 00 & 0.2481 \pm 00 & 0.2341 & 00 & 0.2341 & 00 \\ 29 & 0.400 \pm 00 & 0.2481 \pm 00 & 0.2341 & 00 & 0.2341 & 00 \\ 31 & 0.400 \pm 00 & 0.4481 \pm 00 & 0.2341 & 00 & 0.2341 & 00 \\ 32 & 0.400 \pm 00 & 0.4481 \pm 00 & 0.1341 \pm 00 & 0.2341 & 00 \\ 33 & 0.400 \pm 00 & 0.431 \pm 00 & 0.1341 \pm 00 & 0.1341 \pm 00 \\ 33 & 0.400 \pm 00 & 0.431 \pm 00 & 0.1341 \pm 00 & 0.1341 \pm 00 \\ 34 & 0.400 \pm 00 & 0.431 \pm 00 & 0.1341 \pm 00 & 0.1341 \pm 00 \\ 34 & 0.400 \pm 00 & 0.431 \pm 00 & 0.1341 \pm 00 & 0.1341 \pm 00 \\ 34 & 0.400 \pm 00 & 0.431 \pm 00 & 0.1341 \pm 00 & 0.1341 \pm 00 \\ 34 & 0.400 \pm 00 & 0.431 \pm 00 & 0.1341 \pm 00 & 0.1341 \pm 00 \\ 34 & 0.400 \pm 00 & 0.400 \pm 00 & 0.1341 \pm 00 & 0.1341 \pm 00 \\ 34 & 0.400 \pm 00 & 0.400 \pm 00 & 0.331 \pm 00 & 0.4341 \pm 00 \\ 34 & 0.400 \pm 00 & 0.400 \pm 00 & 0.331 \pm 00 & 0.4341 \pm 00 \\ 34 & 0.400 \pm 00 & 0.400 \pm 00 & 0.3341 \pm 00 & 0.1341 \pm 00 \\ 34 & 0.400 \pm 00 & 0.400 \pm 00 & 0.3341 \pm $	12	0.2000 00	0.4936 00	0.1912 00	0.7675-01	0.3502-01		
$\begin{array}{c} 14 & 0.7426 = 01 & 0.7426 = 00 & 0.7426 = 00 & 0.7146 = 00 & 0.7256 = 01 \\ 15 & 0.7357 = 02 & 0.7266 = 00 & 0.7375 = 00 & 0.7757 = 00 & 0.7928 = 01 \\ 16 & 0.1067 = 02 & 0.7366 = 00 & 0.7375 = 00 & 0.1756 = 00 & 0.1066 = 00 \\ 18 & 0.1035 = 03 & 0.2446 = 00 & 0.7336 = 00 & 0.126 = 00 & 0.1196 = 00 \\ 19 & 0.0005 = 00 & 0.1426 = 00 & 0.7336 = 00 & 0.2266 = 00 & 0.1325 = 00 \\ 20 & 0.0005 = 00 & 0.1426 = 00 & 0.7325 = 01 & 0.2365 = 00 & 0.1565 = 00 \\ 21 & 0.0005 = 00 & 0.7255 = 01 & 0.2316 = 00 & 0.2526 = 00 & 0.1575 = 00 \\ 22 & 0.0005 = 00 & 0.7255 = 01 & 0.2316 = 00 & 0.2526 = 00 & 0.1575 = 00 \\ 23 & 0.0005 = 00 & 0.7255 = 01 & 0.2316 = 00 & 0.2526 = 00 & 0.1575 = 00 \\ 24 & 0.0005 = 00 & 0.7255 = 01 & 0.2236 = 00 & 0.2356 = 00 & 0.1955 = 00 \\ 25 & 0.0005 = 00 & 0.1305 = 01 & 0.2236 = 00 & 0.2356 = 00 & 0.2316 = 00 \\ 26 & 0.0005 = 00 & 0.1305 = 01 & 0.2236 = 00 & 0.2336 = 00 & 0.2316 = 00 \\ 26 & 0.0005 = 00 & 0.1305 = 01 & 0.1755 = 00 & 0.2235 = 00 & 0.2336 = 00 \\ 26 & 0.0005 = 00 & 0.1755 = 0.1 & 0.2356 = 00 & 0.2316 = 00 \\ 26 & 0.0005 = 00 & 0.1755 = 0.1 & 0.1755 = 00 & 0.2316 = 00 & 0.2316 = 00 \\ 27 & 0.0005 = 00 & 0.1755 = 0.1 & 0.1755 = 00 & 0.2316 = 00 & 0.2316 = 00 \\ 28 & 0.0005 = 00 & 0.1265 = 0.3 & 0.1425 = 00 & 0.2316 = 00 & 0.2316 = 00 \\ 28 & 0.0005 = 00 & 0.1265 = 0.3 & 0.1425 = 00 & 0.1375 = 00 & 0.1376 = 00 \\ 31 & 0.0005 = 00 & 0.1265 = 0.3 & 0.1375 = 00 & 0.1375 = 00 & 0.1376 = 00 \\ 32 & 0.0005 = 00 & 0.1025 = 0.3 & 0.1375 = 00 & 0.1375 = 00 & 0.1376 = 00 \\ 33 & 0.0005 = 00 & 0.1025 = 0.3 & 0.1375 = 00 & 0.1376 = 00 \\ 33 & 0.0005 = 00 & 0.1025 = 0.3 & 0.1375 = 0.0 & 0.1376 = 00 \\ 34 & 0.0005 = 00 & 0.1025 = 0.1 & 0.1325 = 00 & 0.1376 = 00 \\ 34 & 0.0005 = 00 & 0.0005 = 00 & 0.1325 = 0.0 & 0.1365 = 00 \\ 34 & 0.0005 = 00 & 0.0005 = 00 & 0.1375 = 0.0 & 0.1365 = 00 \\ 34 & 0.0005 = 00 & 0.0005 = 00 & 0.1375 = 0.0 & 0.1375 = 0.0 \\ 34 & 0.0005 = 00 & 0.0005 = 00 & 0.1375 = 0.0 & 0.1375 = 0.0 \\ 34 & 0.0005 = 00 & 0.0005 = 00 & 0.1375 = 0.0 & 0.1375 = 0.0 \\ 44 & 0.0005 = 00 & 0.0005 = 00 & 0.1375 = 0.0 &$	12	0.4205-01	0.5096 00	0.2410 00	0.4586-01	0.4482-01		
$ \begin{array}{c} 13 & 0.433 = -02 & 0.4227 & 00 & 0.4312 & 00 & 0.4371 & 00 & 0.4928 = 01 \\ 16 & 0.4061 - 02 & 0.5661 & 00 & 0.4326 & 00 & 0.4372 & 00 & 0.4928 = 01 \\ 17 & 0.4301 - 03 & 0.3028 & 00 & 0.5376 & 00 & 0.4226 & 00 & 0.4192 & 00 \\ 18 & 0.4031 - 03 & 0.2464 & 00 & 0.4326 & 00 & 0.4226 & 00 & 0.1426 & 00 \\ 20 & 0.0006 & 00 & 0.1426 & 00 & 0.3316 & 00 & 0.2266 & 00 & 0.1646 & 00 \\ 21 & 0.0006 & 00 & 0.1426 & 00 & 0.3326 & 00 & 0.2466 & 00 & 0.1666 & 00 \\ 22 & 0.0006 & 00 & 0.1226 & 00 & 0.2326 & 00 & 0.1676 & 00 \\ 23 & 0.0006 & 00 & 0.7256 - 01 & 0.2256 & 00 & 0.2546 & 00 & 0.1676 & 00 \\ 23 & 0.0006 & 00 & 0.4726 - 01 & 0.2256 & 00 & 0.2546 & 00 & 0.1776 & 00 \\ 24 & 0.0006 & 00 & 0.3276 - 01 & 0.2226 & 00 & 0.2536 & 00 & 0.1977 & 00 \\ 25 & 0.0006 & 00 & 0.1301 - 01 & 0.2226 & 00 & 0.2536 & 00 & 0.1977 & 00 \\ 27 & 0.0006 & 00 & 0.1301 - 01 & 0.2226 & 00 & 0.2536 & 00 & 0.2016 & 00 \\ 28 & 0.0006 & 00 & 0.1301 - 01 & 0.2226 & 00 & 0.2236 & 00 & 0.2016 & 00 \\ 29 & 0.0006 & 00 & 0.1466 - 02 & 0.1306 & 00 & 0.2236 & 00 & 0.2016 & 00 \\ 29 & 0.0006 & 00 & 0.1466 - 02 & 0.1301 & 00 & 0.2026 & 00 \\ 31 & 0.0006 & 00 & 0.1466 - 02 & 0.6361 - 10 & 0.1776 & 00 & 0.2026 & 00 \\ 33 & 0.0006 & 00 & 0.2161 - 0 & 0.1261 & 00 & 0.2026 & 00 \\ 33 & 0.0006 & 00 & 0.2161 - 0 & 0.1316 & 00 & 0.1966 & 00 \\ 33 & 0.0006 & 00 & 0.2161 - 0 & 0.1676 & 00 & 0.1966 & 00 \\ 33 & 0.0006 & 00 & 0.2161 - 0 & 0.1316 & 00 & 0.1864 & 00 \\ 33 & 0.0006 & 00 & 0.20261 - 0 & 0.1316 & 00 & 0.1864 & 00 \\ 33 & 0.0006 & 00 & 0.0006 & 00 & 0.1321 - 01 & 0.1316 & 00 & 0.1864 & 00 \\ 33 & 0.0006 & 00 & 0.0006 & 00 & 0.1321 - 01 & 0.1316 & 00 & 0.1864 & 00 \\ 34 & 0.0006 & 00 & 0.0006 & 00 & 0.1321 - 01 & 0.1316 & 00 & 0.1864 & 00 \\ 34 & 0.0006 & 00 & 0.0006 & 00 & 0.13221 - 01 & 0.1316 & 00 & 0.1864 & 00 \\ 34 & 0.0006 & 00 & 0.0006 & 00 & 0.13221 - 01 & 0.1316 & 00 \\ 34 & 0.0006 & 00 & 0.0006 & 00 & 0.13221 - 01 & 0.1316 & 00 \\ 34 & 0.0006 & 00 & 0.0006 & 00 & 0.13221 - 01 & 0.1316 & 00 \\ 34 & 0.0006 & 00 & 0.0006 & 00 & 0.13222 - 01 & 0.1322 - 01 \\ 44 & 0.0006 & 00$	14	0.1585-01	0.4695 00	0.2016 00	0.1365 00	0.4725-01		
$\begin{array}{c} 16 & 0.1601-02 & 0.3344 & 00 & 0.3374 & 00 & 0.1774 & 00 & 0.9284-01 \\ 17 & 0.4381-03 & 0.3334 & 00 & 0.3374 & 00 & 0.3374 & 00 & 0.2124 & 00 & 0.1194 & 00 \\ 19 & 0.0006 & 00 & 0.1484 & 00 & 0.3314 & 00 & 0.2324 & 00 & 0.1444 & 00 \\ 20 & 0.0006 & 00 & 0.1484 & 00 & 0.3314 & 00 & 0.2384 & 00 & 0.1444 & 00 \\ 21 & 0.0006 & 00 & 0.1034 & 00 & 0.2384 & 00 & 0.1464 & 00 \\ 22 & 0.0006 & 00 & 0.7255-01 & 0.2214 & 00 & 0.2324 & 00 & 0.1464 & 00 \\ 23 & 0.0006 & 00 & 0.7255-01 & 0.2214 & 00 & 0.2524 & 00 & 0.1476 & 00 \\ 23 & 0.0006 & 00 & 0.3371-01 & 0.2294 & 00 & 0.2534 & 00 & 0.1476 & 00 \\ 24 & 0.0006 & 00 & 0.3371-01 & 0.2294 & 00 & 0.2534 & 00 & 0.1476 & 00 \\ 25 & 0.0006 & 00 & 0.307-01 & 0.2294 & 00 & 0.2534 & 00 & 0.1976 & 00 \\ 26 & 0.0006 & 00 & 0.106-01 & 0.1756 & 00 & 0.2234 & 00 & 0.1976 & 00 \\ 27 & 0.0006 & 00 & 0.1466-02 & 0.1266 & 00 & 0.2234 & 00 & 0.2016 & 00 \\ 28 & 0.0006 & 00 & 0.4661-02 & 0.1266 & 00 & 0.2234 & 00 & 0.2016 & 00 \\ 28 & 0.0006 & 00 & 0.4661-02 & 0.1266 & 00 & 0.2234 & 00 & 0.2026 & 00 \\ 30 & 0.0006 & 00 & 0.4861-02 & 0.1676 & 00 & 0.2026 & 00 \\ 31 & 0.0006 & 00 & 0.4261-03 & 0.5861-01 & 0.11976 & 00 & 0.2026 & 00 \\ 32 & 0.0006 & 00 & 0.2161-03 & 0.5861-01 & 0.11976 & 00 & 0.1956 & 00 \\ 33 & 0.0006 & 00 & 0.2161-03 & 0.5861-01 & 0.11976 & 00 \\ 33 & 0.0006 & 00 & 0.0216-00 & 0.2216-00 & 0.1186 & 00 & 0.1966 & 00 \\ 33 & 0.0006 & 00 & 0.0006 & 00 & 0.1081-01 & 0.1676 & 00 \\ 33 & 0.0006 & 00 & 0.0006 & 00 & 0.1021-01 & 0.9176 & 00 \\ 33 & 0.0006 & 00 & 0.0006 & 00 & 0.1021-01 & 0.9176 & 00 \\ 33 & 0.0006 & 00 & 0.0006 & 00 & 0.1021-01 & 0.9476 & 00 \\ 33 & 0.0006 & 00 & 0.0006 & 00 & 0.1281-01 & 0.1186 & 00 \\ 44 & 0.0006 & 00 & 0.0006 & 00 & 0.5281-02 & 0.6078-01 & 0.1316 & 00 \\ 44 & 0.0006 & 00 & 0.0006 & 00 & 0.5281-02 & 0.6078-01 & 0.1316 & 00 \\ 44 & 0.0006 & 00 & 0.0006 & 00 & 0.3281-02 & 0.5381-01 & 0.1316 & 00 \\ 44 & 0.0006 & 00 & 0.0006 & 00 & 0.3281-02 & 0.5381-01 & 0.1316 & 00 \\ 44 & 0.0006 & 00 & 0.0006 & 00 & 0.3281-02 & 0.5381-01 & 0.1316 & 00 \\ 44 & 0.0006 & 00 & 0.0006 & 00 & $	15	0.5335-02	0.4225 00	0.3136 00	0.1578 00	0.7985-01		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	16	0.160F-02	0.364E 00	0.3295 00	0.1776 00	0.9285-01		
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	17	0.430E-03	0.303E 00	0.337E 00	0.1955 00	0.106E 00		
$\begin{array}{c} 19 & 0.4000E 00 & 0.148E 00 & 0.333E 00 & 0.224E 00 & 0.132E 00 \\ 20 & 0.400E 00 & 0.143E 00 & 0.333E 00 & 0.238E 00 & 0.154E 00 \\ 21 & 0.400E 00 & 0.143E 00 & 0.238E 00 & 0.154E 00 \\ 22 & 0.400E 00 & 0.495E-01 & 0.254E 00 & 0.254E 00 & 0.167E 00 \\ 23 & 0.400E 00 & 0.327E-01 & 0.226E 00 & 0.254E 00 & 0.167E 00 \\ 24 & 0.400E 00 & 0.327E-01 & 0.226E 00 & 0.236E 00 & 0.167E 00 \\ 25 & 0.400E 00 & 0.327E-01 & 0.226E 00 & 0.236E 00 & 0.167E 00 \\ 26 & 0.400E 00 & 0.139E-01 & 0.202E 00 & 0.236E 00 & 0.167E 00 \\ 27 & 0.400E 00 & 0.139E-01 & 0.276E 00 & 0.237E 00 & 0.276E 00 \\ 28 & 0.400E 00 & 0.446E-02 & 0.156E 00 & 0.232E 00 & 0.201E 00 \\ 28 & 0.400E 00 & 0.446E-02 & 0.126E 00 & 0.223E 00 & 0.201E 00 \\ 30 & 0.400E 00 & 0.446E-02 & 0.167E 00 & 0.223E 00 \\ 31 & 0.400E 00 & 0.446E-02 & 0.167E 00 & 0.202E 00 \\ 32 & 0.400E 00 & 0.446E-02 & 0.167E 00 & 0.202E 00 \\ 33 & 0.400E 00 & 0.446E-02 & 0.546E-01 & 0.167E 00 & 0.202E 00 \\ 33 & 0.400E 00 & 0.446E-02 & 0.546E-01 & 0.167E 00 & 0.202E 00 \\ 33 & 0.400E 00 & 0.421E-03 & 0.427E-01 & 0.151E 00 & 0.169E 00 \\ 34 & 0.000E 00 & 0.421E-03 & 0.427E-01 & 0.151E 00 & 0.169E 00 \\ 35 & 0.400E 00 & 0.400E 00 & 0.102E-01 & 0.136E 00 & 0.167E 00 \\ 35 & 0.400E 00 & 0.400E 00 & 0.102E-01 & 0.162E 00 & 0.164E 00 \\ 36 & 0.400E 00 & 0.400E 00 & 0.102E-01 & 0.164E 00 \\ 37 & 0.400E 00 & 0.400E 00 & 0.428E-01 & 0.162E 00 \\ 38 & 0.400E 00 & 0.400E 00 & 0.428E-01 & 0.162E 00 \\ 38 & 0.400E 00 & 0.400E 00 & 0.428E-01 & 0.164E 00 \\ 40 & 0.400E 00 & 0.400E 00 & 0.428E-01 & 0.164E 00 \\ 42 & 0.400E 00 & 0.400E 00 & 0.428E-01 & 0.164E 00 \\ 44 & 0.400E 00 & 0.400E 00 & 0.428E-02 & 0.434E-01 & 0.154E 00 \\ 44 & 0.400E 00 & 0.400E 00 & 0.428E-01 & 0.164E 00 \\ 44 & 0.400E 00 & 0.400E 00 & 0.428E-01 & 0.164E 00 \\ 44 & 0.400E 00 & 0.400E 00 & 0.428E-01 & 0.164E 00 \\ 44 & 0.400E 00 & 0.400E 00 & 0.428E-01 & 0.164E 00 \\ 44 & 0.400E 00 & 0.400E 00 & 0.428E-01 & 0.164E 00 \\ 44 & 0.400E 00 & 0.400E 00 & 0.428E-01 & 0.164E 00 \\ 44 & 0.400E 00 & 0.400E 00 & 0.428E-01 & 0.164E 00 \\ 44 & 0.400E 00 & 0.400E 00 & 0.4$	18	0.103E-03	0.244E 00	0.3398 00	0.212E 00	0.119F 00		
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	19	0.000E 00	0.189E 00	0.333E 00	0.226E 00	0.132E 00		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	20	0.000E 00	0.142E 00	0.321E 00	0.238E 00	0.144E 00		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	21	0.000E 00	0.103E 00	0.303E 00	0.246E 00	0.156E 00	· · · · · · · · · · · · · · · · · · ·	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	22	0.000E 00	0.7256-01	0.281E 00	0.252E 00	0.167E 00		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	23	0.000E 00	0.495E-01	0.256E 00	0.254E 00	0.177E 00		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	24	0.000E 00	0.3275-01	0.229E 00	0.253E 00	0.185E 00		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	25	0.000E 00	0.210E-01	0.202E 00	0.250E 00	0.192E 00		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	26	0.000E 00	0.130E-01	0.175E 00	0.243E 00	0.197E 00		
$\begin{array}{c} 23 & 0.000E 00 & 0.266E-02 & 0.126E 00 & 0.223E 00 & 0.203E 00 \\ 30 & 0.000E 00 & 0.146E-02 & 0.654E-01 & 0.197E 00 & 0.202E 00 \\ 31 & 0.000E 00 & 0.421E-03 & 0.668E-01 & 0.182E 00 & 0.200E 00 \\ 32 & 0.000E 00 & 0.421E-03 & 0.468E-01 & 0.182E 00 & 0.199E 00 \\ 33 & 0.000E 00 & 0.215E-03 & 0.427E-01 & 0.151E 00 & 0.199E 00 \\ 34 & 0.000E 00 & 0.107E-03 & 0.360E-01 & 0.136E 00 & 0.196E 00 \\ 35 & 0.000E 00 & 0.000E 00 & 0.251E-01 & 0.122E 00 & 0.176E 00 \\ 36 & 0.000E 00 & 0.000E 00 & 0.168E-01 & 0.166E 00 \\ 37 & 0.000E 00 & 0.000E 00 & 0.168E-01 & 0.166E 00 \\ 38 & 0.000E 00 & 0.000E 00 & 0.102E-01 & 0.623E-01 & 0.150E 00 \\ 40 & 0.000E 00 & 0.000E 00 & 0.746E-02 & 0.710E-01 & 0.141E 00 \\ 40 & 0.000E 00 & 0.000E 00 & 0.372E-02 & 0.607E-01 & 0.131E 00 \\ 41 & 0.000E 00 & 0.000E 00 & 0.372E-02 & 0.507E-01 & 0.121E 00 \\ 42 & 0.000E 00 & 0.000E 00 & 0.120E-02 & 0.306E-01 & 0.102E 00 \\ 43 & 0.000E 00 & 0.000E 00 & 0.177E-02 & 0.362E-01 & 0.102E 00 \\ 44 & 0.000E 00 & 0.000E 00 & 0.120E-02 & 0.306E-01 & 0.102E 00 \\ 44 & 0.000E 00 & 0.000E 00 & 0.132E-02 & 0.306E-01 & 0.102E 00 \\ 44 & 0.000E 00 & 0.000E 00 & 0.132E-02 & 0.306E-01 & 0.102E 00 \\ 44 & 0.000E 00 & 0.000E 00 & 0.372E-02 & 0.306E-01 & 0.102E 00 \\ 45 & 0.000E 00 & 0.000E 00 & 0.372E-02 & 0.306E-01 & 0.757E-01 \\ 46 & 0.000E 00 & 0.000E 00 & 0.338E-03 & 0.202E-01 & 0.757E-01 \\ 47 & 0.000E 00 & 0.000E 00 & 0.338E-03 & 0.202E-01 & 0.757E-01 \\ 47 & 0.000E 00 & 0.000E 00 & 0.328E-03 & 0.131E-01 & 0.603E-01 \\ 49 & 0.000E 00 & 0.000E 00 & 0.328E-03 & 0.131E-01 & 0.603E-01 \\ 49 & 0.000E 00 & 0.000E 00 & 0.328E-03 & 0.131E-01 & 0.603E-01 \\ 50 & 0.000E 00 & 0.000E 00 & 0.328E-03 & 0.131E-01 & 0.603E-01 \\ 51 & 0.000E 00 & 0.000E 00 & 0.000E 00 & 0.538E-03 & 0.138E-01 \\ 52 & 0.000E 00 & 0.000E 00 & 0.000E 00 & 0.538E-02 & 0.412E-01 \\ 52 & 0.000E 00 & 0.000E 00 & 0.000E 00 & 0.538E-02 & 0.412E-01 \\ 52 & 0.000E 00 & 0.000E 00 & 0.000E 00 & 0.538E-02 & 0.412E-01 \\ 52 & 0.000E 00 & 0.000E 00 & 0.000E 00 & 0.538E-02 & 0.412E-01 \\ 52 & 0.000E 00 & 0.000E 00 & 0.000E 00 & 0.538E-$	27	0.0008 00	0.792E-02	0.150E 00	0.234E 00	0.201E 00		
$\begin{array}{c} 29 & 0.000E 00 & 0.286E-02 & 0.014E 00 & 0.211E 00 & 0.202E 00 \\ 31 & 0.000E 00 & 0.48E-02 & 0.684E-01 & 0.182E 00 & 0.202E 00 \\ 32 & 0.000E 00 & 0.421E-03 & 0.546E-01 & 0.182E 00 & 0.202E 00 \\ 33 & 0.000E 00 & 0.421E-03 & 0.546E-01 & 0.167E 00 & 0.195E 00 \\ 34 & 0.000E 00 & 0.107E-03 & 0.330E-01 & 0.136E 00 & 0.184E 00 \\ 35 & 0.000E 00 & 0.000E 00 & 0.251E-01 & 0.122E 00 & 0.176E 00 \\ 36 & 0.000E 00 & 0.000E 00 & 0.148E-01 & 0.107E 00 & 0.168E 00 \\ 37 & 0.000E 00 & 0.000E 00 & 0.146E-01 & 0.947E-01 & 0.160E 00 \\ 38 & 0.000E 00 & 0.000E 00 & 0.140E-01 & 0.947E-01 & 0.160E 00 \\ 39 & 0.000E 00 & 0.000E 00 & 0.140E-01 & 0.823E-01 & 0.150E 00 \\ 40 & 0.000E 00 & 0.000E 00 & 0.258E-02 & 0.67E-01 & 0.141E 00 \\ 41 & 0.000E 00 & 0.000E 00 & 0.258E-02 & 0.516E-01 & 0.121E 00 \\ 42 & 0.000E 00 & 0.000E 00 & 0.258E-02 & 0.434E-01 & 0.112E 00 \\ 44 & 0.000E 00 & 0.000E 00 & 0.258E-02 & 0.434E-01 & 0.112E 00 \\ 44 & 0.000E 00 & 0.000E 00 & 0.258E-02 & 0.434E-01 & 0.112E 00 \\ 44 & 0.000E 00 & 0.000E 00 & 0.258E-02 & 0.434E-01 & 0.102E 00 \\ 44 & 0.000E 00 & 0.000E 00 & 0.258E-02 & 0.434E-01 & 0.102E 00 \\ 44 & 0.000E 00 & 0.000E 00 & 0.258E-02 & 0.434E-01 & 0.102E 00 \\ 44 & 0.000E 00 & 0.000E 00 & 0.258E-02 & 0.434E-01 & 0.102E 00 \\ 45 & 0.000E 00 & 0.000E 00 & 0.258E-03 & 0.202E-01 & 0.930E-01 \\ 45 & 0.000E 00 & 0.000E 00 & 0.533E-03 & 0.202E-01 & 0.6842E-01 \\ 46 & 0.000E 00 & 0.000E 00 & 0.338E-03 & 0.202E-01 & 0.638E-01 \\ 47 & 0.000E 00 & 0.000E 00 & 0.258E-03 & 0.163E-01 & 0.638E-01 \\ 49 & 0.000E 00 & 0.000E 00 & 0.258E-03 & 0.163E-01 & 0.638E-01 \\ 49 & 0.000E 00 & 0.000E 00 & 0.028E-03 & 0.163E-01 & 0.638E-01 \\ 50 & 0.000E 00 & 0.000E 00 & 0.000E 00 & 0.832E-03 & 0.105E-01 \\ 50 & 0.000E 00 & 0.000E 00 & 0.000E 00 & 0.632E-03 & 0.138E-01 & 0.638E-01 \\ 50 & 0.000E 00 & 0.000E 00 & 0.000E 00 & 0.538E-03 & 0.105E-01 \\ 50 & 0.000E 00 & 0.000E 00 & 0.000E 00 & 0.538E-02 & 0.470E-01 \\ 50 & 0.000E 00 & 0.000E 00 & 0.000E 00 & 0.538E-02 & 0.470E-01 \\ 50 & 0.000E 00 & 0.000E 00 & 0.000E 00 & 0.538E-02 & 0.470E-01 \\ 50 & 0.000E 0$	28	0.000E 00	0.466E-02	0.126E 00	0.223E 00	0.203E 00		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	29	0.000E 00	0.2668-02	0.1048 00	0.2118 00	0.203E 00		
$\begin{array}{c} 31 & 0.000 & 00 & 0.4216 - 03 & 0.6886 - 01 & 0.1876 & 00 & 0.2006 & 00 \\ 32 & 0.0006 & 00 & 0.4216 - 03 & 0.5366 - 01 & 0.1676 & 00 & 0.1956 & 00 \\ 33 & 0.0006 & 00 & 0.0006 & 00 & 0.4216 - 01 & 0.1516 & 00 & 0.1966 & 00 \\ 34 & 0.0006 & 00 & 0.0006 & 00 & 0.2516 - 01 & 0.1226 & 00 & 0.1766 & 00 \\ 35 & 0.0006 & 00 & 0.0006 & 00 & 0.1886 - 01 & 0.1076 & 00 & 0.1686 & 00 \\ 37 & 0.0006 & 00 & 0.0006 & 00 & 0.140E - 01 & 0.4276 - 01 & 0.1606 & 00 \\ 38 & 0.0006 & 00 & 0.0006 & 00 & 0.140E - 01 & 0.4976 - 01 & 0.1606 & 00 \\ 39 & 0.0006 & 00 & 0.0006 & 00 & 0.7406 - 02 & 0.7106 - 01 & 0.1416 & 00 \\ 40 & 0.0006 & 00 & 0.0006 & 00 & 0.5286 - 02 & 0.6076 - 01 & 0.1316 & 00 \\ 41 & 0.0006 & 00 & 0.0006 & 00 & 0.2586 - 02 & 0.6076 - 01 & 0.1216 & 00 \\ 42 & 0.0006 & 00 & 0.0006 & 00 & 0.2586 - 02 & 0.6076 - 01 & 0.1216 & 00 \\ 43 & 0.0006 & 00 & 0.0006 & 00 & 0.1776 - 02 & 0.3626 - 01 & 0.1026 & 00 \\ 44 & 0.0006 & 00 & 0.0006 & 00 & 0.1776 - 02 & 0.3626 - 01 & 0.1026 & 00 \\ 44 & 0.0006 & 00 & 0.0006 & 00 & 0.1776 - 02 & 0.3626 - 01 & 0.1026 & 00 \\ 44 & 0.0006 & 00 & 0.0006 & 00 & 0.3076 - 03 & 0.2476 - 01 & 0.8426 - 01 \\ 45 & 0.0006 & 00 & 0.0006 & 00 & 0.336 - 03 & 0.2476 - 01 & 0.8426 - 01 \\ 46 & 0.0006 & 00 & 0.0006 & 00 & 0.336 - 03 & 0.2476 - 01 & 0.8426 - 01 \\ 46 & 0.0006 & 00 & 0.0006 & 00 & 0.336 - 03 & 0.2476 - 01 & 0.8426 - 01 \\ 47 & 0.0006 & 00 & 0.0006 & 00 & 0.336 - 03 & 0.2476 - 01 & 0.8426 - 01 \\ 46 & 0.0006 & 00 & 0.0006 & 00 & 0.336 - 03 & 0.2476 - 01 & 0.8426 - 01 \\ 47 & 0.0006 & 00 & 0.0006 & 00 & 0.336 - 03 & 0.318 - 01 & 0.6036 - 01 \\ 49 & 0.0006 & 00 & 0.0006 & 00 & 0.3256 - 02 & 0.4706 - 01 \\ 49 & 0.0006 & 00 & 0.0006 & 00 & 0.8326 - 02 & 0.4706 - 01 \\ 50 & 0.0006 & 00 & 0.0006 & 00 & 0.8326 - 02 & 0.4706 - 01 \\ 51 & 0.0006 & 00 & 0.0006 & 00 & 0.0006 & 00 & 0.5336 - 01 \\ 52 & 0.0006 & 00 & 0.0006 & 00 & 0.5316 - 02 & 0.4706 - 01 \\ 52 & 0.0006 & 00 & 0.0006 & 00 & 0.55116 - 02 & 0.3596 - 01 \\ 52 & 0.0006 & 00 & 0.0006 & 00 & 0.55116 - 02 & 0.3596 - 01 \\ 52 & 0.0006 & 00 & 0.0006 & 00 & 0.55116 - $	30	0.0002 00	0.148E-02	0.8545-01	0.1978 00	0.202E 00		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	32	0.0005 00	0.60000-03	0.6665-01	0.1828 00	0.2006 00		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	33	0.0005 00	0.2155-03	0.6275-01	0.1676 00	0.1996 00		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	34	0.000E 00	0.1076-03	0.3305-01	0.1366 00	0.1906 00		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	35	0.0005 00	0.000F 00	0.2516-01	0.1228 00	0.1766 00		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	36	0.000F 00	0.000E 00	0.1886-01	0.1075 00	0.1685 00		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	37	0.000E 00	0.000E 00	0.140E-01	0.9476-01	0.160E 00		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	38	0.000E 00	0.000E 00	0.1028-01	0.823E-01	0.150E 00	· · · · · · · · · · · · · · · · · · ·	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	39	0.000E 00	0.000E 00	0.7406-02	0.710E-01	0.141E 00		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	40	0.000E 00	0.000E 00	0.528E-02	0.607E-01	0.131E 00		1.123
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	41	0.000E 00	0.000E 00	0.3728-02	0.516E-01	0.121E 00		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	42	0.000E 00	0.000E 00	0.2588-02	0.4346-01	0.111E 00		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	43	0.0008 00	0.000E 00	0.1776-02	0.3626-01	0.102E 00		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	44	0.000E 00	0.000E 00	0.120E-02	0.300E-01	0.930E-01		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	45	0.000E 00	0.000E 00	0.807E-03	0.247E-01	0.8426-01		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	46	0.000E 00	0.000E 00	0.533E-03	0.2028-01	0.7576-01		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	47	0.0000 00	0.000E 00	0.3482-03	0.163E-01	0.678E-01		
47         0.000E 00         0.000E 00         0.143E-03         0.105E-01         0.534E-01           50         0.000E 00         0.000E 00         0.000E 00         0.832E-02         0.470E-01           51         0.000E 00         0.000E 00         0.654E-02         0.412E-01           52         0.000E 00         0.000E 00         0.511E-02         0.359E-01         24	40	0.0000 00	0.000E 00	0.1425-03	0.1312-01	0.603E-01		
51       0.000E       00       0.000E       00       0.000E       00       0.654E-02       0.412E-01         52       0.000E       00       0.000E       00       0.000E       00       0.511E-02       0.359E-01	4 Y 5 A	0.0000 00	0.0000 00	0.1435-03	0.1056-01	0.5346-01		
52 0.000E 00 0.000E 00 0.000E 00 0.511E-02 0.359E-01 24	50	0.0005 00	0.0000 00	0.0005 00	0.6545-02	0.4125-01		
24	52	0.000E 00	0.000E 00	0.000E 00	0.5115-02	0.3596-01		
				VETWNE WW	<b></b>	CONTRACTOR OF		14

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	53	0.0005 00	0.000F 00	0.000F 00	0-396E-02	0-312E-01
	54	0.0005 00	0.0005 00	0.0005 00	0.3055-02	0.2495-01
	G G	0.0005 00	0.0005 00	0.000F 00	0.233E-02	0.2316-01
province & and a classic classical and an entry of the second second second second second second second second	56	0.000F 00	0.000E 00	0.000E 00	0.176E-02	0-198F-01
	57	0.000E 00	0.000E 00	0.000E 00	0.1335-02	0-168E-01
	58	0.000F 00	0.000E 00	0.000E 00	0.9975-03	0-142E-01
	59	0.0005 00	0.000E 00	0.000F 00	0.7405-03	0.120E-01
	60	0.000E 00	0.000E 00	0.000E 00	0.546E-03	0-100F-01
	61	0.000F 00	0.000E 00	0.0005 00	0.400E-03	0-840E-02
	62	0.0005 00	0.000F 00	0.000F 00	0.2915-03	0.698F-02
	63	0.000F 00	0.000F 00	0.000F 00	0.210E-03	0.577E-02
	64	0.0005 00	0.000E 00	0.000E 00	0.151E-03	0-474F-02
	65	0.000F 00	0.000F 00	0.000F 00	0.1076-03	0-388E-02
	66	0.000F 00	0.000F 00	0.000F 00	0.0005 00	0-317E-02
	67	0.000F 00	0.000F 00	0.000E 00	0.0005 00	0.2575-02
	68	0.000E 00	0.000E 00	0.000F 00	0.000E 00	0-207E-02
	69	0.000E 00	0.000E 00	0.0005 00	0.0000 00	0-167E-02
	70	0.0005 00	0.0005 00	0.0005 00	0.0005 00	0-1335-02
	71	0.0000 00	0.000E 00	0.0005 00	0.0005 00	0-1065-02
	73	0.0000 00	0.0005 00	0.0005 00	0.0005 00	0.8455-03
	73	0.0006 00	0.0005 00	0.0005 00	0.0005 00	0-668E-03
	74	0.0005 00	0.0005 00	0.0005 00	0.0006 00	0.5255-03
	75	0.0005 00	0.0000 00	0.0005 00	0.0005 00	0.4115-03
	76	0.0000 00	0.0000 00	0.0000 00	0.0000 00	0.3205-03
	77	0.0005 00	0.0000 00	0.0000 00	0.0005 00	0.2495-03
	78	0.0005 00	0.0006 00	0.0005 00	0.0005 00	0.1925-03
	70	0.0005 00	0.0005 00	0.0005 00	0.0005 00	0-1475-03
	80	0.0000 00	0.0005 00	0.0000 00	0.0000 00	0.1136-03
	81	0.000E 00	0.0005 00	0.0005 00	0.0005 00	0.000E 00
	a 🤉	0.0005 00	0.0005 00	0.0005 00	0.0005 00	0.0005.00
	83	0.0005 00	0.000E 00	0.0000 00	0.0000 00	0.0005 00
· · · · · · · · · · · · · · · · · · ·	94	0.0005 00	0.0005 00	0.0000 00	0.0005 00	0.0005.00
	84	0.0005 00	0.0005 00	0.0005 00	0.0005 00	0.000E 00
	86	0.0000 00	0.0005 00	0.0000 00	0.0005 00	0.0005 00
	87	0.0005 00	0.0005 00	0.0006 00	0.0005 00	0.000E 00
1 <u>* </u>	88	0.0005 00	0.0005 00	0.0005 00	0.0000 00	0.0008.00
	00	0.0000 00	0.0005 00	0.0000 00	0.0000 00	0.0005.00
	0,	0.0000 00	0.0000 00	0.0005 00	0.0005 00	0.0005.00
	01	0.0000 00	0.0005 00	0.0000 00	0.0000 00	0.0005.00
	02	0.0000 00	0.0000 00	0.0006.00	0.0005.00	0.0005.00
	03	0.0006 00	0.0000 00	0.0005 00	0.0005 00	0.0005.00
	40	0.0005 00	0.0005 00	0.0000 00	0.0005 00	0.000F 00
	05	0.0005 00	0.0005 00	0.0006 00	0.0005 00	0.000E 00
	06	0.0005.00	0.0006 00	0.0005 00	0.0005 00	0.0005.00
	07	0.0000 00	0.0000 00	0.0005 00	0.0005 00	0.000F 00
	0.0	0.0005 00	0.0005 00	0.0005 00	0.0005 00	0.0005 00
	90	0.0005 00	0.0005 00	0.0000 00	0.0005 00	0-000E 00
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COMPARISON OF MOST PROBABLE SPEED, AVERAGE SPEED, AND ROOT MEAN SQUARE SPEED OF MAXWELLIAN DISTRIBUTION, AND DISTRIBUTION IN EFFUSIVE FLOW

TYPE OF ATOM IS K MASS= 0.64953E-22GRAMS TEMPERATURE= 450.0DEG. K.

ACCORDING TO MAXWELLIAN DISTRIBUTION, VMP=(2KT/M)**.5, AV=(8KT/3.141M)**.5, RMSV=(3KT/M)**.5

VMP= 0.43734E 05CM/SEC AV= 0.49353E 05CM/SEC RMSV= 0.53563E 05CM/SEC

ACCORDING TO EFFUSIVE FLOW DISTRIBUTION, VMP=(3KT/M)**.5, AV=.75(2*3.141KT/M)**.5, RMSV=(KT/M)**.5

VMP= 0.53563E 05CM/SEC AV= 0.58132E 05CM/SEC RMSV= 0.30924E 05CM/SEC

TIME= 0.280E-02SEC DISTANCE= 0.150E 03CM FOR POINTS 1

TIME= 0.373E-02SEC DISTANCE= 0.200E 03CM FOR POINTS 2

TIME= 0.466E-02SEC DISTANCE= 0.250E 03CM FOR POINTS 3

PLOT OF I VS T ACCORDING TO THE EQUATION I=C(S**3/T**4)*E**(-BS**2/T**2)

INCRE	MENT ALONG X-AXI	S= 0.163000E-	OBSEC, CONST	ANT DISTANCE	UNNORMALIZED	DATA		
STEP	TIME(IN SEC)	POINTS 1	POINTS 2	POINTS 3	POINTS 4	POINTS 5		
1	0.163000E-03	0.000E 00	0.000E 00	0.000E 00			17 · · · ·	
2	0.326000E-03	0.000E 00	0.000E 00	0.000E 00				
 3	0.489000E-03	0.2546-01	0.1456-17	0.000E 00				
i.	0.651999E-03	0.179E 08	0.1916-01	0.358E-13				
5	0.814999E-03	0.155E 12	0.384E 06	0.1526-01				
6	0.977999E-03	0.168E 14	0.279E 10	0.248E 05				
 7	0.114099E-02	0.237E 15	0.498E 12	0.115E 09				
8	0.130399E-02	0.115E 16	0.126E 14	0.243E 11				
9	0.146699E-02	0.308E 16	0.104E 15	0.859E 12				
10	0.162999E-02	0.571E 16	0.432E 15	0.100E 14				
11	0.179299E-02	0.841E 16	0.115E 16	0.582E 14				
12	0.1955998-02	0.106E 17	0.231E 16	0.208E 15				
13	0.211899E-02	0.121E 17	0.376E 16	0.535E 15				
14	0.228199E-02	0.130E 17	0.5318 16	0.108E 16				
 15	0.244499E-02	0.1316 17	0.677E 16	0.184E 16				
16	0.260799E-02	0.129E 17	0.7998 16	0.276E 16				
17	0.277099E-02	0.123E 17	0.890E 16	0.375E 16	Che aller all			
18	0.2933996-02	0.116E 17	0.9518 16	0.473E 16				
19	0.309699E-02	0.107E 17	0.982E 16	0.562E 16				
20	0.325999E-02	0.987E 16	0.989E 16	0.639E 16				
21	0.342299E-02	0.900E 16	0.977E 16	0.699E 16				
22	0.3585996-02	0.817E 16	0.951E 16	0.744E 16				
23	0.374899E-02	0.739E 16	0.914E 16	0.773E 16	S. S. Charles			
24	0.391199E-02	0.668E 16	0.871E 16	0.788E 16				
25	0.407499E-02	0.602E 16	0.823E 16	0.7918 16				
26	0.423799E-02	0.543E 16	0.774E 16	0.785E 16				
27	0.440099E-02	0.490E 16	0.724E 16	0.770E 16				
28	0.456399E-02	0.442E 16	0.675E 16	0.750E 16				
29	0.472699E-02	0.399E 16	0.628E 16	0.725E 16				
30	0.488999E-02	0.360E 16	0.583E 16	0.6968 16				
 31	0.505299E-02	0.326E 16	0.540E 16	0.666E 16				
32	0.521599E-02	0.295E 16	0.501E 16	0.635E 16			11 A. 1	07
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		0.537899E-02	0.268E 16	0.463E 16	0.603E 16	
	34	0.554199E-02	0.243E 16	0.429E 16	0.571E 16	
	32	0.5704996-02	0.2216 16	0.3976 16	0.540E 16	
	27	0.4020005-02	0.1846 14	0.3076 16	0.510E 16	
	38	0.61030995-02	0.1695 16	0.3402 10	0.4800 10	
	20	0.6356996-02	0.1546 16	0.2016 16	0 4926 16	
	40	0.6510005-02	0.1415 16	0.2705 16	0.4200 10	
	41	0.6682996-02	0.1305 16	0.2516 16	0.3766 16	
	42	0.6845995-02	0.1196 16	0.2335 16	0.3546 16	
	43	0.700899E-02	0.110E 16	0.216F 16	0.3325 16	
	la la	0.717199E-02	0.101E 16	0.2016 16	0.3126 16	
	45	0.733499E-02	0.936E 15	0.1876 16	0.294E 16	
	46	0.7497996-02	0.866E 15	0.174E 16	0.276E 16	
	47	0.766099E-02	0.801E 15	0.162E 16	0.259E 16	
	48	0.782399E-02	0.743E 15	0.151E 16	0.244E 16	
	49	0.798699E-02	0.689E 15	0.141E 16	0.230E 16	
	50	0.814999E-02	0.640E 15	0.132E 16	0.2168 16	
	51	0.8312996-02	0.596E 15	0.123E 16	0.203E 16	
	52	0.8475998-02	0.555E 15	0.115E 16	0.192E 16	
	53	0.8638998-02	0.517E 15	0.108E 16	0.181E 16	
	54	0.880199E-02	0.483E 15	0.101E 16	0.170E 16	
· · · · · · · · · · · · · · · · · · ·	55	0.8964996-02	0.451E 15	0.954E 15	0.1618 16	
	56	0.912799E-02	0.422E 15	0.896E 15	0.152E 16	
	57	0.929099E-02	0.395E 15	0.842E 15	0.143E 16	
	58	0.945399E-02	0.370E 15	0.792E 15	0.135E 16	
	59	0.961699E-02	0.347E 15	0.745E 15	0.128E 16	
	60	0.977999E-02	0.326E 15	0.702E 15	0.1218 16	
	61	0.994299E-02	0.3068 15	0.662E 15	0.114E 16	
	62	0.101059E-01	0.2888 15	0.624E 15	0.108E 16	
	63	0.102689E-01	0.271E 15	0.589E 15	0.103E 16	
	04	0.1043198-01	0.255E 15	0.557E 15	0.977E 15	
	60	0.1075706-01	0.2415 15	0.5265 15	0.9265 15	
	67	0.1002096-01	0.2145 15	0.4968 10	0.8/98 15	
	68	0.11092092-01	0 2026 15	0.44710 15	0 7035 15	
	60	0.1124695-01	0.1025 15	0 4226 15	0 7545 15	
	70	0.114099E-01	0.1816 15	0.4016 15	0.7175 15	
	71	0.1157296-01	0.172E 15	0.3816 15	0.6826 15	
	72	0.117359E-01	0.163E 15	0.362E 15	0.649E 15	
	73	0.118989E-01	0.154E 15	0.344E 15	0.6185 15	
	74	0.1206195-01	0.147E 15	0.327E 15	0.589E 15	
	75	0.1222496-01	0.139E 15	0.311E 15	0.562E 15	
	76	0.1238796-01	0.132E 15	0.2966 15	0.5368 15	
	77	0.125509E-01	0.126E 15	0.282E 15	0.5116 15	
	78	0.127139E-01	0.120E 15	0.269E 15	0.488E 15	No. No. and the second s
	79	0.128769E-01	0.114E 15	0.256E 15	0.466E 15	
	80	0.1303996-01	0.108E 15	0.244E 15	0.445E 15	
1	81	0.132029E-01	0.103E 15	0.233E 15	0.4268 15	
	82	0.133659E-01	0.990E 14	0.222E 15	0.4078 15	
	83	0.135289E-01	0.944E 14	0.213E 15	0.390E 15	
	84	0.136919E-01	0.901E 14	0.203E 15	0.373E 15	
1. <u> </u>	85	0.138549E-01	0.861E 14	0.194E 15	0.357E 15	
	86	0.140179E-01	0.823E 14	0.186E 15	0.342E 15	
2	87	0.141809E-01	0.787E 14	0.1788 15	0.3288 15	
	88	0.143439E-01	0.752E 14	0.170E 15	0.314E 15	
	89	0.1450698-01	0.720E 14	0.1638 15	0.302E 15	
	90	0.1400998-01	0.689E 14	0.156E 15	0.2898 15	
	91	0.1483298-01	0.6002 14	0.150E 15	0.2788 15	
	36	0.1444245-01	0.033E 14	0.1445 15	U.267E 15	

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	03	0.1515895-01	0.6075 14	0 1395 15	0 2565 15		
$( \cdot )$	94	0.153219E-01	0.582E 14	0.132E 15	0.246E 15		
-	95	0.154849E-01	0.558E 14	0.127E 15	0.237E 15		
$\left( \begin{array}{c} \\ \end{array} \right)$	97	0.158109E-01	0.515E 14	0.117E 15	0.219E 15		
	98	0.159739E-01	0.494E 14 0.475E 14	0.113E 15	0.211E 15		
$\left( \right)$	100	0.162999E-01	0.457E 14	0.104E 15	0.195E 15		
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RANGE -	0.1005 01	TOP -	0.1005 01	ROTTOM -	0.0005 00	CCALC -	0 1005-01 050 0750	
ILMINGE "	VALUE OF A	XIS IS 0.0	0000 00		0.0002 00	SUALE =	U. LUUE-UL PER STEP	
DATA FOR	PLOTS							
STEP	POINTS 1	POINTS 2	POINTS 3	POINTS 4	POINTS 5			
				101110 4				
1	0.000E 00	0.000E 00	0.000E 00					-
. Z	0.000E 00	0.000E 00	0.000E 00					
3	0.0006 00	0.000E 00	0.0008 00					
	0.0002 00	0.0000 00	0.0000 00					
6	0.127E-02	0.000F 00	0.0000 00					
7	0.179E-01	0.000E 00	0.000E 00					
8	0.875E-01	0.955E-03	0.000E 00	×.		22		
9	0.233E 00	0.788E-02	0.000E 00					2
10	0.432E 00	0.327E-01	0.764E-03					
11	0.637E 00	0.877E-01	0.441E-02					
12	0.807E 00	0.175E 00	0.1576-01					
13	0.923E 00	0.285E 00	0.405E-01					
1 50	0.1005 01	0.5135 00	0.8226-01					
16	0.980F 00	0.6055 00	0.2095 00					
17	0.937E 00	0.674E 00	0.2846 00					
18	0.879E 00	0.720E 00	0.358E 00					
19	0.815E 00	0.744E 00	0.426E 00					
20	0.748E 00	0.750E 00	0.484E 00					
21	0.682E 00	0.740E 00	0.530E 00					a and
22	0.619E 00	0.720E 00	0.563E 00					
23	0.5601 00	0.6928 00	0.5865 00					
24	0.4565 00	0.6396 00	0.5972 00					
26	0.4116 00	0.5865 00	0.5945 00					
27	0.371E 00	0.548E 00	0.5838 00					
28	0.335E 00	0.511E 00	0.568E 00					~
29	0.302E 00	0.476E 00	0.549E 00					1
30	0.273E 00	0.442E 00	0.527E 00					
31	0.247E 00	0.409E 00	0.504E 00					
32	0.224E 00	0.379E 00	0.481E 00					
33	0.2038 00	0.3518 00	0.457E 00					ad a second s
34	0.1648 00	0.325E 00	0.433E 00					
36	0.1535 00	0.2786 00	0.3865 00					
37	0.139E 00	0.257E 00	0.364F 00	,				
38	0.127E 00	0.238E 00	0.3438 00				-	
39	0.117E 00	0.221E 00	0.3228 00					
40	0.107E 00	0.205E 00	0.303E 00					
41	0.985E-01	0.190E 00	0.285E 00					
42	0.905E-01	0.176E 00	0.2688 00					
43	0.8336-01	0.164E 00	0.2528 00					
44	0.7095-01	0.1528 00	0.2378 00					
46	0.6565-01	0.1325 00	0.2005 00					
47	0.607E-01	0.123F 00	0.1965 00					
48	0.563E-01	0.1148 00	0.1858 00					y ×
49	0.522E-01	0.107E 00	0.174E 00					
50	0.4856-01	0.100E 00	0.164E 00					
51	0.451E-01	0.937E-01	0.154E 00					
52	0.420E-01	0.877E-01	0.145E 00					

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	E 73	0 2026 01	0 0005 01	0 1070 00			
	23	0.3925-01	0.8226-01	0.1375 00			
	54	0.3658-01	0.7702-01	0.129E 00			
	22	0.341E-01	0.723E-01	0.1228 00			
	26	0.3196-01	0.679E-01	0.115E 00			
	57	0.299E-01	0.638E-01	0.108E 00			
	58	0.2802-01	0.600E-01	0.102E 00			
	59	0.263E-01	0.565E-01	0.971E-01	$(x,y) \in \mathcal{S}(x) = \mathcal{S}(x) = (x,y) = $		
	60	0.2476-01	0.532E-01	0.919E-01			
	61	0.232E-01	0.501E-01	0.870E-01			
	62	0.218E-01	0.473E-01	0.824E-01			
	63	0.2056-01	0.446E-01	0.780E-01			
	64	0.193E-01	0.422E-01	0.740E-01			
	65	0.1828-01	0.399E-01	0.7026-01			
	66	0.1726-01	0.377E-01	0.666E-01			
	67	0.162E-01	0.357E-01	0.6328-01			
	68	0.153E-01	0.338E-01	0.601E-01			
	69	0.145E-01	0.321E-01	0.571E-01	•		
	70	0.1376-01	0.304E-01	0.543E-01			
	71	0.1306-01	0.289E-01	0.5176-01			
	72	0.1236-01	0.2748-01	0.4926-01			
	73	0.1178-01	0.260E-01	0.468E-01			
	74	0.1116-01	0.247E-01	0.4468-01			
	75	0.105E-01	0.2355-01	0.425E-01			
	76	0.100E-01	0.224E-01	0.4065-01			
	77	0.9566-02	0.213E-01	0-3876-01			
	78	0.909E-02	0-2035-01	0.3705-01			
	79	0-8665-02	0.1946-01	0.3535-01			
	80	0.8256-02	0.1856-01	0.3376-01			
	81	0.7865-02	0.1765-01	0.3226-01			
	82	0.7506-02	0 1485-01	0 3095-01			
	20	0.7156-02	0.1616-01	0.3055-01			
	20	0.6935-02	0.1545-01	0.2925-01			
	95	0.4526-02	0.1476-01	0.2705-01			
	94	0 6225-02	0 1476-01	0.2595-01			
	00	0.6236-02	0 1255-01	0.2096-01			
	01	0.5705-02	0.1356-01	0.2305-01	 		
	00	0.5/02-02	0.1296-01	0.2385-01			
	09	0.5425-02	0.1232-01	0.2288-01	 		
	90	0.522E-02	0.1188-01	0.2196-01			
	31	0.5002-02	0.1138-01	0.2102-01			
	92	0.4/9E-02	0.1095-01	0.2028-01			
	93	0.4602-02	0.1046-01	0.1948-01	 · · · · · · · · · · · · · · · · · · ·		
	94	0.4416-02	0.1008-01	0.1865-01			
	95	0.423E-02	0.966E-02	0.179E-01			
	96	0.4065-02	0.928E-02	0.172E-01			
	97	0.3908-02	0.891E-02	0.166E-01			
	98	0.375E-02	0.857E-02	0.159E-01			
	99	0.360E-02	0.824E-02	0.1538-01			
	100	0.346E-02	0.793E-02	0.1485-01			
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ITE	OF ATOM IS RB	MASS= 0.141	98E-21GRAMS	TEMPERATURE= 450	ODEG. K.	
ACCOP RMSV	RDING TO MAXWELL =(3KT/M)*≈∙5	IAN DISTRIBU	TION, VMP=(2KT	/M)**.5, AV=(8KT	/3.141M)**.5,	
VMP=	0.29580E 05CM/S	EC AV= 0.3	3381E 05CM/SEC	RMSV= 0.36228	E OSCM/SEC	
ACCOF AV=.1	RDING TO EFFUSIV 75(2*3.141KT/M)*	E FLOW DISTR *.5, RMSV=(K	IBUTION, VMP=( T/M)**.5	3KT/M)**.5,		
VMP=	0.36228E 05CM/S	EC AV= 0.3	9319E 05CM/SEC	RMSV= 0.20916	E OSCM/SEC	
TIME	• 0.414E-02SEC	DISTANCE=	0.150E 03CM	FOR POINTS 1		
TIME	= 0.552E-02SEC	DISTANCE=	0.200E 03CM	FOR POINTS 2		
TIME	= 0.690E-02SEC	DISTANCE=	0.250E 03CM	FOR POINTS 3		
PLOT	OF I VS T ACCOR	DING TO THE I	EQUATION I=C(S	**3/T**4)*E**(-B	5**2/T**2)	
INCRE	EMENT ALONG X-AX	IS= 0.241999	E-03SEC,CON	STANT DISTANCE	UNNORMALIZED DATA	
STEP	TIME(IN SEC)	POINTS 1	POINTS 2	POINTS 3	POINTS 4 POI	TS 5
1	0.241999E-03	0.000E 00	0.000E 00	0.000E 00		
2	0.483999E-03	0.000E 00	0.0005 00	0.000E 00		
3	0.725999E-03	0.789E-02	0.621E-18	0.000E 00		
4	0.967999E-03	0.464E 07	0.5925-02	0.139E-13		
5	0.120999E-02	0.371E 11	0.102E 06	0.473E-02		
6	0.145199E-02	0.383E 13	0.689E 09	0.680E 04		
1	0.169399E-02	0.526E 14	0.117E 12	0.2948 08		
• 0	0.1935996-02	0.2518 15	0.2878 13	0.5888 10		
10	0.21/7996-02	0.663E 15	0.232E 14	0.200E 12		
10	0.2419996-02	0.1705 14	0.9508 14	0.2305 13		
12	0.2001992-02	0.2245 16	0.4076 15	0.1302 14		
13	0.3145996-02	0.2565 16	0.8056 15	0-1175 15		
14	0.338799E-02	0.272F 16	0.1135 16	0.2355 15		
15	0.3629996-02	0.276E 16	0.1435 16	0.3985 15		
16	0.387199E-02	0.270E 16	0.168E 16	0.592E 15		
17	0.411399E-02	0.257E 16	0.187E 16	0.801E 15		
18	0.435599E-02	0.241E 16	0.1998 16	0.100E 16		
19	0.459799E-02	0.223E 16	0.205E 16	0.119E 16		
20	0.483999E-02	0.205E 16	0.207E 16	0.134E 16	100 million -	
21	0.508199E-02	0.186E 16	0.204E 16	0.147E 16		
22	0.532399E-02	0.169E 16	0.198E 16	0.156E 16		
23	0.556599E-02	0.153E 16	0.190E 16	0.162E 16		
24	0.580799E-02	0.138E 16	0.181E 16	0.165E 16		
25	0.604999E-02	0.124E 16	0.171E 16	0.165E 16		
26	0.6291998-02	0.112E 16	0.160E 16	0.164E 16		
27	0.653399E-02	0.101E 16	0.150E 16	0.160E 16		
28	0.677599E-02	0.914E 15	0.140E 16	0.156E 16		
2734 and	0.701799E-02	0.825E 15	0.130E 16	0.151E 16		
29	the the second second second second	275 CT 255 CT 255				
29	0.725999E-02	0.745E 15	0.1208 16	0.1458 16		
29 30 31	0.725999E-02 0.750199E-02	0.745E 15 0.674E 15	0.120E 16 0.112E 16	0.145E 16 0.138E 16		

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3	34	0.8227996-02	0.503E 15	0.888E 15	0.118E 16	
	35	0.846999E-02	0.458E 15	0.8218 15	0.112E 16	
	36	0.871199E-02	0.417E 15	0.760E 15	0.105E 16	
	37	0.895399E-02	0.380E 15	0.703E 15	0.997E 15	
	38	0.919599E-02	0.348E 15	0.6518 15	0.938E 15	
	39	0.943799E-02	0.318E 15	0.603E 15	0.883E 15	
	40	0.967999E-02	0.292E 15	0.559E 15	0.830E 15	
	41	0.992199E-02	0.268E 15	0.5188 15	0.780E 15	
	42	0.101639E-01	0.246E 15	0.481E 15	0.733E 15	
	43	0.104059E-01	0.226E 15	0.447E 15	0.688E 15	
	44	0.106479E-01	0.209E 15	0.415E 15	0.647E 15	
	45	0.108899E-01	0.193E 15	0.3868 15	0.608E 15	
	46	0.111319E-01	0.178E 15	0.360E 15	0.571E 15	
	47	0.113739E-01	0.165E 15	0.335E 15	0.537E 15	
	48	0.116159E-01	0.153E 15	0.313E 15	0.505E 15	
	49	0.118579E-01	0.1428 15	0.292E 15	0.475E 15	
	50	0.120999E-01	0.132E 15	0.2736 15	0.4478 15	
	51	0.123419E-01	0.122E 15	0.255E 15	0.421E 15	
	52	0.125839E-01	0.114E 15	0.239E 15	0.396E 15	
	53	0.128259E-01	0.106E 15	0.2238 15	0.374E 15	
	54	0.130679E-01	0.995E 14	0.2098 15	0.352E 15	
	55	0.133099E-01	0.930E 14	0.196E 15	0.332E 15	
	56	0.135519E-01	0.869E 14	0.184E 15	0.313E 15	
	57	0.137939E-01	0.814E 14	0.173E 15	0.296E 15	
	58	0.140359E-01	0.763E 14	0.163E 15	0.280E 15	
	59	0.142779E-01	0.715E 14	0.153E 15	0.264E 15	
	60	0.145199E-01	0.672E 14	0.144E 15	0.250E 15	
	61	0.147619E-01	0.631E 14	0.136E 15	0.237E 15	
	62	0.150039E-01	0.594E 14	0.128E 15	0.2248 15	
	63	0.152459E-01	0.559E 14	0.1216 15	0.212E 15	
	64	0.154879E-01	0.526E 14	0.114E 15	0.201E 15	
	65	0.157299E-01	0.496E 14	0.108E 15	0.1916 15	
	66	0.159719E-01	0.468E 14	0.102E 15	0.181E 15	
	67	0.162139E-01	0.442E 14	0.9728 14	0.1728 15	
	68	0.164559E-01	0.418E 14	0.9216 14	0.163E 15	
	69	0.166979E-01	0.395E 14	0.873E 14	0.155E 15	
	70	0.169399E-01	0.374E 14	0.828E 14	0.147E 15	
	71	0.171819E-01	0.354E 14	0.786E 14	0.140E 15	
	72	0.174239E-01	0.336E 14	0.746E 14	0.133E 15	
	73	0.176659E-01	0.319E 14	0.7098 14	0.127E 15	
	74	0.179079E-01	0.302E 14	0.674E 14	0.121E 15	
	75	0.181499E-01	0.287E 14	0.641E 14	0.115E 15	
	76	0.183919E-01	0.273E 14	0.610E 14	0.1108 15	
	77	0.186339E-01	0.259E 14	0.581E 14	0.105E 15	
	78	0.188759E-01	0.247E 14	0.554E 14	0.1006 15	
	79	0.191179E-01	0.235E 14	0.5288 14	0.962E 14	
	80	0.193599E-01	0.224E 14	0.504E 14	0.919E 14	
	81	0.196019E-01	0.213E 14	0.481E 14	0.878E 14	
	82	0.198439E-01	0.203E 14	0.459E 14	0.840E 14	
	83	0.200859E-01	0.194E 14	0.438E 14	0.804E 14	
	84	0.203279E-01	0.185E 14	0.4198 14	0.769E 14	
	85	0.205699E-01	0.177E 14	0.401E 14	0.737E 14	
	86	0.208119E-01	0.169E 14	0.383E 14	0.706E 14	
	87	0.210539E-01	0.162E 14	0.367E 14	0.676E 14	
	88	0.212959E-01	0.155E 14	0.351E 14	0.648E 14	
	89	0.215379E-01	0.148E 14	0.336E 14	0.622E 14	
	90	0.217799E-01	0.142E 14	0.322E 14	0.597E 14	
	91	0.220219E-01	0.136E 14	0.309E 14	0.573E 14	
	92	0.222639E-01	0.130E 14	0.296E 14	0.550E 14	
	100710 1173	1.2250596-01	0-1255 14	0.784- 14	0.5285 14	

C *								
	94	0.2274796-01	0.119F 14	0.273E 14	0.508F 14			
(California)	95	0.229899E-01	0.115E 14	0.262E 14	0.488E 14			
	97	0.234739E-01	0.110E 14	0.252E 14 0.242E 14	0.469E 14 0.452E 14			
Q _	98	0.237159E-01	0.101E 14	0.233E 14	0.435E 14			
	100	0.241999E-01	0.941E 13	0.215E 14	0.418E 14 0.403E 14	•		
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	<u></u>	Sec. Sugar	Jan Strange	Section of the last			A CONTRACTOR	35

	RANGE =	0.100E 01	TOP =	0.100E 01	BOTTOM =	0.000E	00	SCALE =	0.1008-01	PER STEP	
		VALUE UF A	XIS IS 0.0	000 00			and the second				
C	DATA FOR	PLOTS	4								
	CTCO.	ODINTS 1	DOTATE 2	DOTNES 3	DOTNE A	BOINTO	z				
	SICF	PUINISI	PUINTS 2	PUINIS 3	PUINIS 4	PUINIS	2				
	1	0.000E 00	0.000E 00	0.000E 00							
	2	0.000E 00	0.000E 00	0.000E 00					•		
	3	0.000E 00	0.000E 00	0.000E 00							
	4	0.000E 00	0.000E 00	0.000E 00							
	5	0.000E 00	0.000E 00	0.000E 00							
	6	0.138E-02	0.000E 00	0.000E 00							
	1	0.190E-01	0.000E 00	0.000E 00							
	ð	0.9128-01	0.104E-02	0.000E 00							
	10	0.2406 00	0.3446-02	0.0000000		· · · ·					
	10	0.4410 00	0.9105-01	0.6325-03							
	12	0-814E 00	0.180F 00	0-1665-01							
	13	0.928E 00	0.291E 00	0.424E-01							
	14	0.987E 00	0.409E 00	0.851E-01							· · · · · · · · · · · · · · · · · · ·
No.	15	0.100E 01	0.519E 00	0.144E 00							
	16	0.978E 00	0.610E 00	0.214E 00							
	17	0.933E 00	0.679E 00	0.290E 00							
	18	0.875E 00	0.723E 00	0.364E 00							
	19	0.810E 00	0.745E 00	0.431E 00			the second s			~	
	20	0.743E 00	0.749E 00	0.488E 00							
	21	0.6762 00	0.739E 00	0.533E 00							
	22	0.6142 00	0.718E 00	0.5662 00							
	23	0.5015 00	0.6902 00	0.5870 00							
	25	0.451E 00	0.6205 00	0.6005 00							
	26	0.407E 00	0.582E 00	0.5946 00						ar en en en dar i falle et fan haar het en de fan en de te en en en en de fan een en en de fan het en en dar ha	ann an start an ann an thar ann an
	27	0.367E 00	0.544E 00	0.582E 00							
	28	0.331E 00	0.507E 00	0.566E 00							
	29	0.298E 00	0.472E 00	0.5468 00							
	30	0.270E 00	0.438E 00	0.525E 00							
	31	0.244E 00	0.405E 00	0.502E 00							
	32	0.221E 00	0.375E 00	0.478E 00							
	33	0.200E 00	0.347E 00	0.453E 00				the second s			
	34	0.182E 00	0.3218 00	0.429E 00							
	35	0.1656 00	0.2978 00	0.4068 00				-		-	
	20	0.1376 00	0.2545 00	0.3636 00							
	38	0.1265 00	0.2355 00	0.3395 00							
	30	0.1156 00	0.2185 00	0.3195 00							
	40	0.105E 00	0.202E 00	0.300E 00							
	41	0.971E-01	0.187E 00	0.282E 00							
1	42	0.892E-01	0.174E 00	0.265E 00							
	43	0.8216-01	0.161E 00	0.249E 00							
	le le	0.757E-01	0.150E 00	0.234E 00							
	45	0.699E-01	0.140E 00	0.220E 00			1				
	46	0.646E-01	0.130E 00	0.207E 00							
	47	0.5986-01	0.121E 00	0.194E 00							
	48	0.5546-01	0.113E 00	0.1838 00							
	47	0.0795-01	0.1056 00	0.1425 00							
	51	0.4446-01	0.9245-01	0.1525 00							
	52	0.414E-01	0.865E-01	0.143E 00							
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2	53	0.386E-01	0.810E-01	0.135E 00	 
	54	0.360E-01	0.760E-01	0.127E 00	
	55	0.336E-01	0.713E-01	0.120E 00	
	56	0.314E-01	0.669E-01	0.113E 00	
	57	0.294E-01	0.629E-01	0.107E 00	
	58	0.276E-01	0.5916-01	0.101E 00	
	59	0.259E-01	0.5576-01	0.959E-01	
	60	0.243E-01	0.524E-01	0.907E-01	
	61	0.2286-01	0.494E-01	0.8586-01	
	62	0.2156-01	0.466E-01	0.812E-01	
	63	0-202E-01	0.440E-01	0.7705-01	
	64	0.190F-01	0.4165-01	0.7305-01	
	65	0.1795-01	0.3936-01	0.6925-01	
	66	0.1695-01	0.3725-01	0.6575-01	
	67	0 1605-01	0 3525-01	0.6376-01	
	49	0.1515-01	0.3326-01	0.60250-01	
	60	0 1438-01	0.3332-01	0.5425-01	
	70	0.1436-01	0.3100-01	0.5635-01	
	70	0.1356-01	0.2996-01	0.5352-01	
	/1	0.1285-01	0.2846-01	0.509E-01	
	12	0.121E-01	0.270E-01	0.485E-01	
	73	0.115E-01	0.256E-01	0.462E-01	 
	74	0.109E-01	0.244E-01	0.440E-01	
	75	0.104E-01	0.232E-01	0.419E-01	 *
	76	0.9896-02	0.2216-01	0.400E-01	
	77	0.941E-02	0.210E-01	0.382E-01	
	78	0.895E-02	0.200E-01	0.364E-01	
	79	0.852E-02	0.191E-01	0.348E-01	
	80	0.812E-02	0.182E-01	0.332E-01	
	81	0.774E-02	0.174E-01	0.318E-01	· · · · · ·
2	82	0.738E-02	0.166E-01	0.3045-01	
	83	0.704E-02	0-158E-01	0-2915-01	
	84	0.6725-02	0.1516-01	0-2785-01	
	25	0.6425-02	0.1455-01	0-2665-01	
	86	0.6135-02	0.1386-01	0.2555-01	
	00	0.6045-02	0 1225-01	0.2455-01	
	60	0.5415-02	0.1275-01	0.2255-01	
	00	0.5012-02	0.1276-01	0.2356-01	
	69	0.5376-02	0.1212-01		
	90	0.5142-02	0.1166-01	0.2162-01	
	91	0.4925-02	0.1122-01	0.207E-01	 
	72	0.4728-02	0.107E-01	0.1335-01	
	8.8	0.4526-02	0.103E-01	0.1918-01	 
	94	0.434E-02	0.990E-02	0.184E-01	
	95	0.416E-02	0.951E-02	0.176E-01	 
	96	0.400E-02	0.913E-02	0.170E-01	
	97	0.384E-02	0.878E-02	0.163E-01	
	98	0.369E-02	0.844E-02	0.1576-01	
	99	0.3546-02	0.811E-02	0.151E-01	
	100	0.341E-02	0.781E-02	0.146E-01	
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TYPE OF ATOM IS CS MASS= 0.22080E-21GRAMS TEMPERATURE= 450.0DEG. K.

ACCORDING TO MAXWELLIAN DISTRIBUTION, VMP=(2KT/M)**.5, AV=(8KT/3.141M)**.5, RMSV=(3KT/M)**.5

VMP= 0.23720E 05CM/SEC AV= 0.26768E 05CM/SEC RMSV= 0.29051E 05CM/SEC

ACCORDING TO EFFUSIVE FLOW DISTRIBUTION, VMP=(3KT/M)**.5, AV=.75(2*3.141KT/M)**.5, RMSV=(KT/M)**.5

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VMP= 0.29051E 05CM/SEC AV= 0.31529E 05CM/SEC RMSV= 0.16772E 05CM/SEC

TIME= 0.516E-02SEC DISTANCE= 0.150E 03CM FOR POINTS 1

TIME= 0.688E-02SEC DISTANCE= 0.200E 03CM FOR POINTS 2

TIME= 0.860E-02SEC DISTANCE= 0.250E 03CM FOR POINTS 3

PLOT OF I VS T ACCORDING TO THE EQUATION I=C(S**3/T**4)*E**(-BS**2/T**2)

	INCRE	MENT ALONG X-AXI	S= 0.300999E-	O3SEC,CONST	ANT DISTANCE	UNNORMALIZED	DATA	
	STEP	TIME(IN SEC)	POINTS 1	POINTS 2	POINTS 3	POINTS 4	POINTS 5	
	1	0.300999E-03	0.000E 00	0.000E 00	0.000E 00			
	2	0.601999E-03	0.000E 00	0.000E 00	0.000E 00			
	3	0.902999E-03	0.2558-02	0.164E-18	0.000E 00			
	4	0.1203996-02	0.168E 07	0.191E-02	0.391E-14			
	5	0.150499E-02	0.141E 11	0.364E 05	0.153E-02			
	6	0.180599E-02	0.150E 13	0.257E 09	0.237E 04			
	7	0.210699E-02	0.209E 14	0.450E 11	0.107E 08			
-	8	0.240799E-02	0.101E 15	0.112E 13	0.222E 10			
	9	0.2708996-02	0.269E 15	0.922E 13	0.774E 11			
	10	0.3009995-02	0.497E 15	0.381E 14	0.901E 12			
	11	0.331099E-02	0.731E 15	0.101E 15	0.517E 13			
	12	0.361199E-02	0.925E 15	0.202E 15	0.1848 14			
	13	0.3912996-02	0.105E 16	0.328E 15	0.4718 14	- Carlo Carlos and	an like in the	
	14	0.421399E-02	0.112E 16	0.4638 15	0.951E 14			
	15	0.451499E-02	0.114E 16	0.588E 15	0.1618 15			
	16	0.481599E-02	0.111E 16	0.6936 15	0.2418 15			
	17	0.511699E-02	0.106E 16	0.772E 15	0.327E 15			
	18	0.541799E-02	0.100E 16	0.824E 15	0.412E 15			
	19	0.571899E-02	0.928E 15	0.850E 15	0.4898 15			
	20	0.601999E-02	0.852E 15	0.856E 15	0.5558 15			
	21	0.632099E-02	0.777E 15	0.8458 15	0.6078 15			
	22	0.662199E-02	0.705E 15	0.822E 15	0.6458 15			
	23	0.692299E-02	0.637E 15	0.790E 15	0.670E 15			
	24	0.722399E-02	0.575E 15	0.752E 15	0.6828 15			
	25	0.7524995-02	0.519E 15	0.710E 15	0.685E 15			
	26	0.782599E-02	0.468E 15	0.668E 15	0.6798 15			
	27	0.812699E-02	0.422E 15	0.6258 15	0.666E 15			
	28	0.842799E-02	0.380E 15	0.582E 15	0.648E 15			
	29	0.872899E-02	0.343E 15	0.542E 15	0.626E 15			
	30	0.902999E-02	0.310E 15	0.503E 15	0.601E 15			
	31	0.933099E-02	0.281E 15	0.466E 15	0.575E 15			
	32	0.963199E-02	0.254E 15	0.431E 15	0.548E 15			
	33	0.993299E-02	0.231E 15	0.399E 15	0.520E 15		The second second	

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	34	0.102339E-01	0.210E 15	0.369E 15	0.493E 15	
C	35	0.105349E-01	0.191E 15	0.342E 15	0.466E 15	
property and the second	36	0.108359E-01	0.174E 15	0.316E 15	0.440E 15	
	37	0.111369E-01	0.158E 15	0.293E 15	0.414E 15	
<u> </u>	38	0.114379E-01	0.145E 15	0.271E 15	0.3908 15	
	39	0.117389E-01	0.132E 15	0.2518 15	0.367E 15	
	40	0.120399E-01	0.121E 15	0.233E 15	0.3456 15	
ξ	41	0.123409E-01	0.111E 15	0.2168 15	0.3246 15	
	42	0.126419E-01	0.102E 15	0.2008 15	0.3056 15	
	43	0.1294296-01	0.947E 14	0.1365 15	0.2868 15	
C	64 64 1 C	0.1324398-01	0.8738 14	0.1/3E 15	0.2696 15	
	40	0.1354492-01	0.8066 14	0.1616 15	0.2535 15	
/	40	0.1384595-01	0.7456 14	0.1405.15	0.2386 15	
$\langle $	4 ( 	0.1414896-01	0.6396 14	0.1305 15	0.2236 15	
	40	0.1444795-01	0.5036 14	0.1216.15	0 1005 15	
	47 E0	0.1504095-01	0.5936 14	0 1126 15	0 1040 15	
(	50	0.1525005-01	0 5175 14	0.1045 15	0.1755 15	
	21 60	0.1545105-01	0.5128 14	0.0076 14	0 1455 15	
	52	0.1505205-01	0 4455 14	0.9345 14	0 1555 15	
C	50	0.1425205-01	0.4155 14	0.9340 14	0 1475 15	
	<u> </u>	0 1655695-01	0 2005 14	0.0756 14	0 1395 15	
	55	0.1685506-01	0 3435 14	0.7716 14	0.1306.15	
(	50	0.1715696-01	0.3405 14	0.7256 14	0.1235 15	
	5.9	0.1745796-01	0.318F 14	0.6826 14	0-1165 15	
	50	0.177589F-01	0.298E 14	0.6415 14	0.110E 15	
C	60	0.180599E-01	0.280E 14	0.604E 14	0.104E 15	
	61	0-183609E-01	0.263E 14	0.570E 14	0.9888 14	
C	62	0.186619E-01	0.248E 14	0.537E 14	0.936E 14	· · · · · ·
	63	0.189629E-01	0.233E 14	0.507E 14	0.887E 14	
	64	0.192639E-01	0.220E 14	0.479E 14	0.841E 14	
( ) -	65	0.195649E-01	0.207E 14	0.453E 14	0.797E 14	
	66	0.198659E-01	0.195E 14	0.428E 14	0.757E 14	
	67	0.201669E-01	0.184E 14	0.406E 14	0.718E 14	
(	68	0.204679E-01	0.174E 14	0.384E 14	0.682E 14	
	69	0.207689E-01	0.165E 14	0.364E 14	0.649E 14	
	70	0.210699E-01	0.156E 14	0.345E 14	0.617E 14	
C	71	0.213709E-01	0.148E 14	0.328E 14	0.587E 14	
	72	0.216719E-01	0.140E 14	0.311E 14	0.559E 14	
	73	0.219729E-01	0.133E 14	0.296E 14	0.532E 14	
C	74	0.222739E-01	0.126E 14	0.281E 14	0.507E 14	
	75	0.225749E-01	0.120E 14	0.267E 14	0.483E 14	
	76	0.228759E-01	0.114E 14	0.255E 14	0.461E 14	
C	77	0.2317695-01	0.108E 14	0.242E 14	0.440E 14	
-	78	0.234779E-01	0.103E 14	0.231E 14	0.420E 14	
	19	0.237789E-01	0.983E 13	0.220E 14	0.401E 14	
C	80	0.240799E-01	0.936E 13	0.210E 14	0.3835 14	
	81	0.243809E-01	0.893E 13	0.200E 14	0.366E 14	
	82	0.2468198-01	0.851E 13	0.1916 14	0.3506 14	
63	83	0.2498296-01	0.8126 13	0.1836 14	0.3355 14	
	04	0.2528396-01	0.7405 13	0.1475.14	0 2075 14	
<i>(</i> .	02	0.2599695-01	0.7096 13	0.1606 14	0.2046 14	
<u> </u>	00	0.2618695-01	0.6775 12	0.1636 14	0.2825 14	
	01	0.2648705-01	0.6475 13	0.1445 14	0.2705 14	
· ·	00 00	0.2678895-01	0.6195 13	0.1405 14	0.2596 14	
n C .	00	0.2708995-01	0.5936 13	0.134F 14	0.2495 14	
	91	0.2739095-01	0.568E 13	0.129F 14	0.239E 14	
(	92	0.2769195-01	0.544E 13	0.123E 14	0.229E 14	
	93	0.279929E-01	0.522E 13	0.118E 14	0.220E 14	
		THE ATO ATOM STRUCTURE AND A TOWNER AND A TOWNER AND A TOWNER	5 10 4 50 C 1 4 50 C 1 50 C 10 C 10 C 10 C 10 C 10 C 10	A LAN DA PERSONAL DA CAL COMPANY	a liter supervised and a liter of the	40

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	94	0.282939E-01	0.5008 13	0.114E 14	0.212E 14		
-	96	0.283949E-01 0.288959E-01	0.4802 13 0.461E 13	0.109E 14	0.1965 14		
5	98	0.291989E-01 0.294979E-01	0.443E 13 0.425E 13	0.101E 14 0.973E 13	0.188E 14 0.181E 14		
_	99 100	0.297989E-01 0.300999E-01	0.409E 13 0.393E 13	0.936E 13 0.901E 13	0.174E 14 0.168E 14		
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	RANGE =	0.100E 01 VALUE OF A	TOP = xis is 0.0	0.100E 01 00E 00	80 <b>TT</b> OM =	0.000E 00	SCALE =	0.100E-01 PER STEP
	DATA FOR	PLOTS					and a second	
	CTCO	OCTATE 1	201476 2	OOTHTO D		COTUTO O		
	SIEP	PUINISI	PUINIS 2	PUINIS 3	PUINIS 4	PUINIS 5		
	1	0.000E 00	0.000E 00	0.000E 00				
	2	0.000E 00	0.000E 00	0.000E 00				
	3	0.000E 00	0.000E 00	0.000E 00				
	64 52	0.000E 00	0.000E 00	0.000E 00				
	6	0.1316-02	0.000E 00	0.000E 00				
	7	0.183E-01	0.000E 00	0.000E 00				
	8	0.888E-01	0.986E-03	0.000E 00				
	9	0.2358 00	0.807E-02	0.000E 00				
	10	0.435E 00	0.8895-01	0.4526-02				
L.	12	0.809E 00	0.176E 00	0.1616-01				
	13	0.925E 00	0.287E 00	0.412E-01				
	14	0.985E 00	0.405E 00	0.833E-01				
	15	0.100E 01	0.515E 00	0.1418 00				
	10	0.9792 00	0.607E 00	0.2116 00				
	18	0.878E 00	0.721E 00	0.360F 00				
	19	0.813E 00	0.744E 00	0.428E 00				
	20	0.746E 00	0.749E 00	0.485E 00				
	21	0.680E 00	0.740E 00	0.531E 00				
	22	0.6178 00	0.720E 00	0.564E 00				
	23	0.5046 00	0.6585 00	0.5976 00				
	25	0.454E 00	0.622E 00	0.5998 00				
	26	0.410E 00	0.584E 00	0.594E 00				
	27	0.369E 00	0.547E 00	0.583E 00				
	28	0.333E 00	0.510E 00	0.567E 00				
	30	0.2725 00	0.4446 00	0.5486 00				
	31	0.246E 00	0.408E 00	0.5038 00				
	32	0.2238 00	0.378E 00	0.480E 00				
·,	33	0.202E 00	0.350E 00	0.455E 00				
	34	0.183E 00	0.323E 00	0.431E 00				
	35	0.1575 00	0.2998 00	0.408E 00				
	37	0.139E 00	0.2565 00	0.3636 00				
1.00	38	0.1278 00	0.237E 00	0.341E 00				
	39	0.116E 00	0.220E 00	0.321E 00				
	40	0.106E 00	0.204E 00	0.302E 00				
,	41	0.9795-01	0.189E 00	0.284E 00				
	43	0.8295-01	0.1636 00	0.2516 00				
	44	0.764E-01	0.1518 00	0.236E 00				
	45	0.705E-01	0.141E 00	0.221E 00				
	46	0.652E-01	0.131E 00	0.208E 00				
	41	0.604E-01	0.122E 00	0.1968 00				
	40	0.5195-01	0.1045 00	0.1735 00				
	50	0.482E-01	0.997E-01	0.1638 00			<b>1</b>	
	51	0.449E-01	0.932E-01	0.153E 00	i			
	52	0.4185-01	0.873E-01	0-144E 00				

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23	0.3896-01	0.8172-01	0.136: 00	
24	0.363E-01	0.7662-01	0.128E 00	
	0.3396-01	0.719E-01	0.121E 00	
56	0.317E-01	0.675E-01	0.114E 00	
	0.2976-01	0.634E-01	0.108E 00	
58	0.278E-01	0.597E-01	0.102E 00	
59	0.261E-01	0.562E-01	0.967E-01	
60	0.245E-01	0.529E-01	0.914E-01	
61	0.230E-01	0.499E-01	0.865E-01	
62	0.217E-01	0.470E-01	0.819E-01	
63	0.2046-01	0.444E-01	0.776E-01	
64	0.1926-01	0.419E-01	0.736E-01	
65	0.181E-01	0.397E-01	0.698E-01	
66	0.171E-01	0.375E-01	0.662E-01	
67	0.161E-01	0.355E-01	0.629E-01	
68	0.153E-01	0.336E-01	0.597E-01	
69	0.144E-01	0.319E-01	0.568E-01	
70	0.137E-01	0.302E-01	0.540E-01	
71	0.129E-01	0.287E-01	0.514E-01	
72	0.123E-01	0.272E-01	0.489E-01	
73	0.116E-01	0.259E-01	0.466E-01	
74	0.110E-01	0.246E-01	0.444E-01	
75	0.105E-01	0.234E-01	0.423E-01	
76	0.999E-02	0.223E-01	0.4046-01	
77	0.950E-02	0.212E-01	0.385E-01	
78	0.904E-02	0.202E-01	0.368E-01	
79	0.861E-02	0.193E-01	0.3516-01	
80	0.8208-02	0.1846-01	0.3356-01	
81	0.781E-02	0.175E-01	0.3216-01	
82	0.745E-02	0.167E-01	0.307E-01	
83	0.711E-02	0.160E-01	0.293E-01	
84	0.679E-02	0.1538-01	0.281E-01	
85	0.648E-02	0.146E-01	0.269E-01	
86	0.619E-02	0.140E-01	0.258E-01	
87	0.592E-02	0.134E-01	0.247E-01	
. 88	0.5676-02	0.128E-01	0.2376-01	
89	0.5426-02	0.123E-01	0.2278-01	
90	0.519E-02	0.118E-01	0-218E-01	
91	0.497E-02	0.113E-01	0.2095-01	
92	0.476E-02	0.108E-01	0.2015-01	
93	0-457E-02	0.104E-01	0-1935-01	
94	0.4385-02	0.1005-01	0-1855-01	
95	0-420E-02	0.960E-02	0-1785-01	
96	0.4046-02	0.9225-02	0-1715-01	
97	0.388E-02	0.8865-02	0.165E-01	
98	0.3725-02	0.8525-02	0.1595-01	
99	0.3585-02	0.8195-02	0.1536-01	
100	0.3445-02	0.7885-02	0-1475-01	
100	0.0446-02	0.1006-02	V.ATIC VA	
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# TABULAR DATA FOR A BEAM OF K ATTENUATED BY N2 AT 300.0 DEG. K

TABLE NUMBER 1---TUBE LENGTH= 150.00 CM

VELOCITY---FOR PRESSURES OF (A) 0.1E-04 MMHG (B) 0.1E-05 MMHG (C) 0.1E-06 MMHG

×		1/1(0)	1/1(0)	1/1(0)
THE R PROPERTY AND	0.2191E 05 CM/SEC	0.6922E-04	0.3837E 00	0.9086E 00
	0.3287E 05 CM/SEC	0.7536E-03	0.4872E 00	0.9306E 00
	0.4383E 05 CM/SEC	0.2153E-02	0.5411E 00	0.9404E 00
	0.5479E 05 CM/SEC	0.3757E-02	0.5721E 00	0.9456E 00
	0.6575E 05 CM/SEC	0.5242E-02	0.5915E 00	0.9488E 00
	0.7671E 05 CM/SEC	0.6504E-02	0.6044E 00	0.9508E 00
	0.8767E 05 CM/SEC	0.7535E-02	0.6133E 00	0.9522E 00
	0.9863E 05 CM/SEC	0.8360E-02	0.6197E 00	0.9532E 00
	0.1096E 06 CM/SEC	0.9016E-02	0.6244E 00	0.9540E 00
	0.1206E 06 CM/SEC	0.9538E-02	0.6279E 00	0.9545E 00
	0.1315E 06 CM/SEC	0.9953E-02	0.6306E 00	0.9549E 00

TABLE NUMBER 2--- TUBE LENGTH= 200.00 CM

	VELOCITYFOR PRESSURES	OF (A) 0.1E-04 MMHG	(B) 0.1E-05 MMHG	(C) 0.1E-06 MMHG
		1/1(0)	1/1(0)	1/1(0)
	0.2504E 05 CM/SEC	0.9784E-05	0.3155E 00	0.8910E 00
	0.3617E 05 CM/SEC	0.1166E-03	0.4042E 00	0.9134E 00
	0.4730E 05 CM/SEC	0.3686E-03	0.45358 00	0.9239E 00
	0.5843E 05 CM/SEC	0.6932E-03	0.48316 00	0.9298E 00
	0.6596E 05 CM/SEC	0.9168E-03	0.4968E 00	0.9324E 00
,	0.8069E 05 CM/SEC	0.1314E-02	0.5150E 00	0.9358E 00
	0.9182E 05 CM/SEC	0.1565E-02	0.52418 00	0.9374E 00
	0.1030E 06 CM/SEC	0.1772E-02	0.5307E 00	0.9386E 00
	0.1141E 06 CM/SEC	0.1940E-02	0.5355E 00	0.9394E 00
	0.1252E 06 CM/SEC	0.2075E-02	0.5391E 00	0.9400E 00
	0.1363E 06 CM/SEC	0.2186E-02	0.5419E 00	0.9405E 00

## SUMMARY

It has been shown that the proposed apparatus is feasible theoretically and practically. The physical conditions necessary to obtain good beam intensity are certainly not prohibitive; pressures of  $10^{-7}$  torr are obtainable, as are flight tube lengths of 150.0 cm to 200.0 cm. Not only that, but there are no new methods used, just a recombination of old ones into a fresh pattern.









// JOB	3
// FOR	NORD INTEGERS
* UNE * EXTE	NORD INTEGERS
* IDCS	S(CARD, 1403 PRINTER, TYPEWRITER)
** ROE	BERT M. HENES CHEMISTRY 272 TIME CONSTANT
	DIMENSION S(20),T(20),S1(101)
	WRITE(5,100)
1	READ(2,101) ANAME, AMASS, ATEMK
	IF(AMASS-99.9)300,301,300
300	WRITE(5,102) ANAME, AMASS, ATEMK
	PI=3.141
	B=AMASS/(2.0*AK*ATEMK)
	Z=AK*ATEMK/AMASS
	$VMP = (2 \cdot 0 + Z) + + \cdot 5$ $VA = (2 \cdot 0 + Z) + + \cdot 5$
	VRMS=(3.0*Z)**.5
	WRITE(5,103)
	WRITE(5,104) VMP,VA,VRMS
	WRITE(5,105)
	VA2=(.75*(2.0*PI*Z)**.5)
	VRMS2=Z**.5
	WRITE(5,104)VMP2,VA2,VRMS2
	B166=0.0
	READ(2,108) S(1)
	IF(S(I)-99.9)12,3,12
12	IF(S(I)-BIGG)2,2,13
13	BIGG=S(I)
3	J=I-1
	DD 4 K=1,J
4	V(K) = S(K) / VMP2 WRITE(5,109) T(K), S(K), 12
	WRITE(5,106)
	\$1(1)=0.0
	LS = (BIGG * 3.5/100.0) + .5
	WS=LS WRITE(5-110) OS
	BBIG=0.0
	WRITE(5,111)
	DO 6 M=1,100
	MM=M DD 7 K=1.1
	AI(K,M)=(S1(M)**3/T(K)**4)*EXP(-B*S1(M)**2/T(K)**2)
	IF(AI(K,M)-BBIG) 7,7,31
31	BBIG=AI(K,M)
,	WRITE(5,112)MM,S1(M),(AI(K,M),K=1,J)
6	S1(M+1) = S1(M) + QS
	DO 30 K=1,J
	$\frac{1}{2} M = 1,100$
	IF(AI(K,M)-1.0E-04) 14,32.32
14	AI(K,M)=0.0
32	CONTINUE
50	- CONTINUE 77

```
CALL PLT02(J,100)
   WRITE(5,116)
    WRITE(1,113)
   PAUSE 1
   CALL DATSW(2,NNN)
   GO TO (1,72),NNN
 72 DO 8 K=1,J
   J2 = 1
   BBIG=0.0
   S1(1)=0.0
    IS=(S(K)*3.5/100.0)+.5
    AS = IS
    WRITE(5,102) ANAME, AMASS, ATEMK
   WRITE(5,109)T(K),S(K),J2
    WRITE(5,106)
    WRITE(5,110) AS
    WRITE(5,115)
   DO 9 M=1,100
    MM = M
    AI(K,M)=(S1(M)**3/T(K)**4)*EXP(-B*S1(M)**2/T(K)**2)
    IF(AI(K,M)-BBIG)20,20,21
 21 BBIG=AI(K,M)
 20 WRITE(5,114)MM,S1(M),AI(K,M)
 9 S1(M+1)=S1(M)+AS
   DO 60 M=1,100
    AI(K,M) = AI(K,M) / BBIG
    IF(AI(K,M)-1.0E-04) 33,60,60
 33 AI(K,M)=0.0
 60 CONTINUE
   CALL PLT02(1,100)
    WRITE(5,116)
  8 CONTINUE
   GO TO 1
301 CALL EXIT
100 FORMAT('ICOMPARISON OF MOST PROBABLE SPEED, AVERAGE SPEED, AND ',
   1'ROOT MEAN SQUARE SPEED OF ',/,' MAXWELLIAN DISTRIBUTION, AND ',
   2'DISTRIBUTION IN EFFUSIVE FLOW')
101 FORMAT(A2,1XE11.4,1XF4.0)
102 FORMAT('OTYPE OF ATOM IS ',A2,' MASS=',E12.5,'GRAMS
                                                              ۰.
   1'TEMPERATURE=', F6.1, 'DEG. K.')
103 FORMAT('OACCORDING TO MAXWELLIAN DISTRIBUTION, VMP=(2KT/M)**.5,',
   1' AV=(8KT/3.141M)**.5, '/,' RMSV=(3KT/M)**.5')
104 FORMAT('OVMP=',E12.5, CM/SEC AV=',E12.5, CM/SEC RMSV=',
   1E12.5, 'CM/SEC')
105 FORMAT('OACCORDING TO EFFUSIVE FLOW DISTRIBUTION, ',
   1 VMP=(3KT/M) ** . 5, ', /, ' AV=. 75(2*3.141KT/M) **.5, RMSV=(KT/M) **.5')
106 FORMAT('OPLOT OF I VS S ACCORDING TO THE EQUATION',
   1' I=C(S**3/T**4)*E**(-BS**2/T**2)')
108 FORMAT(E8.2)
109 FORMAT('OTIME=', E11.3, 'SEC DISTANCE=', E11.3, 'CM FOR POINTS',
   112,/)
110 FORMAT('OINCREMENT ALONG X-AXIS=', F5.1, 'CM, --- CONSTANT TIME',
   1'
         UNNORMALIZED DATA !)
111 FORMAT( STEP DISTANCE(IN CM)
                                                               ۰,
                                    POINTS 1
                                                    POINTS 2
   1'POINTS 3
                   POINTS 4
                            POINTS 5')
112 FORMAT(' ', I4, 7XF5.1, 7XE10.3, 4(4XE10.3))
113 FORMAT('DATSW NO. 2 DOWN FOR INDIVIDUAL GRAPHS, UP FOR SKIPPING',
   1. INDIVIDUAL GRAPHS, PUSH START.
114 FORMAT(' ',14,7XF5.1,7XE10.3)
115 FORMAT(' STEP DISTANCE(IN CM) POINTS 1')
                                                                       50
116 FORMAT('1')
```

0 13	END
	5)

// FOR		
* ONE WORD	INTEGERS	
* EXTENDED	PRECISION	영화 방송 가슴 방송 방송 방송 방송 방송 방송 방송
* IUCSTCARD	1403 PRINTER, ITPEWRITER	
** ROBERT M.	HENES CHEMISTRY	272 DISTANCE CONSTANT
DIMEN	SION S(20), T(20), T1(101)	
	N AI(5,100)	
1 READ(2	2,101) ANAME, AMASS, ATEMK	
IF(AM)	455-99.91300,301,300	
300 WRITE	(5,102) ANAME, AMASS, ATEMK	
PI=3.	141	
B=AMA	SS/(2.0*AK*ATEMK)	
Z=AK*.	ATEMK/AMASS	
VMP=() VA=(8	2.0#2)##.5 0#7/01)## 5	
VRMS=	(3.0*Z)**.5	
WRITE	(5,103)	
WRITE	(5,104) VMP,VA,VRMS	
VMP2=	VRMS	
VA2=(	•75*(2.0*PI*Z)**.5)	
VRMS2	=Z**.5	
BIGG	0-0	
D0 2	I=1,20	
READ (	2,108) S(I)	
	1)-99.9)2,3,2 NUE	
3 J=I-1		
DO 4	K=1,J	
J2=K T(K)=	SIKI /VMD2	
IF(T)	K)-BIGG)4,4,13	
13 BIGG=	Т(К)	
4 WRITE	(5,109) T(K),S(K),J2	
LS=((	BIGG*3.5/100.0)/1.0E-06)+.	5
QS=1.	0E-06*LS	
T1(1)	=QS	
BBIG=	0.0	
WRITE	(5,111)	
DO 6	M=1,100	
DO 7	K=1.J	
AI(K,	M)=(S(K)**3/T1(M)**4)*EXP(	-B*S(K)**2/T1(M)**2)
IF(AI	(K,M)-BBIG) 7,7,31	
31 BB1G= 7 CONTI	AI(K,M) NUE	
WRITE	(5,112)MM,T1(M),(AI(K,M),K	=1,J)
6 T1(M+	1)=T1(M)+QS	
DU 30	N=1,J M=1,100	
AI(K,	M)=AI(K,M)/BBIG	
IF(AI	(K,M)-1.0E-04) 14,32,32	
14 AI(K, 32 CONTI	MJ=0.0 NUE	
30 CONTI	NUE	52

```
CALL PLT02(J,100)
    WRITE(5,116)
    WRITE(1,113)
    PAUSE 1
    CALL DATSW(2,NNN)
    GO TO (1,72), NNN
 72 DO 8 K=1,J
    J_{2}=1
    BBIG=0.0
    IS=((T(K)*3.5/100.0)/1.0E-06)+.5
    AS=1.0E-06#IS
    T1(1) = AS
    WRITE(5,102)ANAME, AMASS, ATEMK
    WRITE(5,109)T(K),S(K),J2
    WRITE(5,106)
    WRITE(5,110) AS
    WRITE(5,115)
    DO 9 M=1,100
    MM = M
    AI(K,M)=(S(K)**3/T1(M)**4)*EXP(-B*S(K)**2/T1(M)**2)
    IF(AI(K,M)-BBIG)20,20,21
 21 BBIG=AI(K,M)
 20 WRITE(5,114)MM,T1(M),AI(K,M)
  9 T1(M+1)=T1(M)+AS
    DO 60 M=1,100
    AI(K,M) = AI(K,M) / BBIG
    IF(AI(K,M)-1.0E-04) 33,60,60
 33 AI(K,M)=0.0
60 CONTINUE
    CALL PLT02(1,100)
    WRITE(5,116)
  8 CONTINUE
    GO TO 1
301 CALL EXIT
100 FORMAT('ICOMPARISON OF MOST PROBABLE SPEED, AVERAGE SPEED, AND ',
   1'ROOT MEAN SQUARE SPEED OF ',/,' MAXWELLIAN DISTRIBUTION, AND ',
   2'DISTRIBUTION IN EFFUSIVE FLOW')
101 FORMAT(A2,1XE11.4,1XF4.0)
102 FORMAT('OTYPE OF ATOM IS ',A2,' MASS=',E12.5,'GRAMS
                                                              ۰,
   1'TEMPERATURE=', F6.1, 'DEG. K.')
103 FORMAT('OACCORDING TO MAXWELLIAN DISTRIBUTION, VMP=(2KT/M)**.5, ',
   1 AV=(8KT/3.141M)**.5, '/,' RMSV=(3KT/M)**.5')
104 FORMAT('OVMP=',E12.5,'CM/SEC AV=',E12.5,'CM/SEC RMSV=',
   1E12.5, 'CM/SEC')
105 FORMAT('OACCORDING TO EFFUSIVE FLOW DISTRIBUTION, ',
   1 VMP=(3KT/M)**.5, ',/,' AV=.75(2*3.141KT/M)**.5, RMSV=(KT/M)**.5')
106 FORMAT('OPLOT OF I VS T ACCORDING TO THE EQUATION',
   1 I=C(S**3/T**4)*E**(-BS**2/T**2))
108 FORMAT(E8.2)
109 FORMAT('OTIME=',E11.3,'SEC
                                  DISTANCE=', E11.3, 'CM FOR POINTS',
   112./)
110 FORMAT('OINCREMENT ALONG X-AXIS=',E13.6,'SEC,---CONSTANT',
   1 DISTANCE
                  UNNORMALIZED DATA · )
111 FORMAT(' STEP
                   TIME(IN SEC)
                                      POINTS 1
                                                                   ۰.
                                                    POINTS 2
   1'POINTS 3
                   POINTS 4
                                  POINTS 5')
112 FORMAT(' ', I4, 2XE13.6, 3XE10.3, 4(4XE10.3))
113 FORMAT('DATSW NO. 2 DOWN FOR INDIVIDUAL GRAPHS, UP FOR SKIPPING',
   1' INDIVIDUAL GRAPHS, PUSH START.')
114 FORMAT(' ', I4, 2XE13.6, 3XE10.3)
115 FORMAT( . STEP
                    TIME(IN SEC)
                                    POINTS 1.)
116 FORMAT('1')
                                                                       53
```



and a second second

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// FOR
* LIST ALL
* ONE WORD INTEGERS
* EXTENDED PRECISION
# IOCS(CARD, 1403 PRINTER)
** ROBERT M. HENES
                           CHEMISTRY 272
                                            I/I(0)
      DIMENSION VEL(2,11), ANG(3), ALEN(2), ALAM(2,3,11), AITI(2,3,11),
     1PSI(2,11), PRE(3)
      AK=1.38E-16
      PI=3.141
      A1=.070523078
      A2=.042282012
      A3=.009270527
      A4=.000152014
      A5=.000276567
      A6=.000043063
      FAC1=SQRT(PI)
      FAC2=2.0/FAC1
      READ(2,100) TEMP, AMG, QEFF
      ALPHA=SQRT((2.0*AK*TEMP)/AMG)
      READ(2,101) NAME1, NAME2
      READ(2, 102)(ALEN(I), I=1, 2)
      READ(2,103)(PRE(I),I=1,3)
      DO 2 I=1,3
      PRESA=(PRE(I)/760.0)*1.01E 06
    2 ANG(I)=PRESA/(AK*TEMP)
      READ(2,104)((VEL(I,J),I=1,2),J=1,11)
      DO 3 I=1,2
      DO 4 J=1,11
      X=VEL(I,J)/ALPHA
      DENO=(1.0+A1*X+A2*X**2+A3*X**3+A4*X**4+A5*X**5+A6*X**6)**16
      ERF=FAC2*(1.0-(1.0/DENO))
    4 PSI(I,J)=(X*EXP(-X**2))+((2.0*X**2+1.0)*ERF)
    3 CONTINUE
      DO 5 I=1,2
      DO 6 J = 1,3
      DO 7 K=1,11
      ALAM(I,J,K)=FAC1*(VEL(I,K)/ALPHA)**2/(ANG(J)*QEFF*PSI(I,K))
    7 AITI(I, J, K) = EXP(-ALEN(I)/ALAM(I, J, K))
    6 CONTINUE
    5 CONTINUE
      WRITE(5,105) NAME1, NAME2, TEMP
      DO 8 I=1,2
      M1 = I
      WRITE(5,106) M1,ALEN(I)
      WRITE(5,107)(PRE(L),L=1,3)
      WRITE(5,108)
      DO 9 K=1,11
    9 WRITE(5,109) VEL(1,K),(AITI(1,J,K),J=1,3)
      WRITE(5,110)
    8 CONTINUE
  100 FORMAT(F5.1,1XE10.4,1XE10.4)
  101 FORMAT(A3,1XA3)
  102 \text{ FORMAT(F6.2,1XF6.2)}
  103 FORMAT(E7.1,2(1XE7.1))
  104 FORMAT(E10.4,1XE10.4)
  105 FORMAT('1',18X'TABULAR DATA FOR A BEAM OF',A3,' ATTENUATED BY',A3,
     1' AT', F6.1, ' DEG. K',/////)
  106 FORMAT(' ', 30X'TABLE NUMBER', 12, '---TUBE LENGTH=', F7.2, ' CM', ///)
  107 FORMAT( ' ,9X'VELOCITY --- FOR PRESSURES OF (A)'E8.1, ' MMHG
                                                                      (B)',
     1E8.1, 'MMHG (C)', E8.1, 'MMHG', //)
                                                                            55
```

108 FORMAT(' '39X'I/I(0)',13X'I/I(0)',13X'I/I(0)')
109 FORMAT(' '4XE11.4,' CM/SEC',15XE11.4,2(8XE11.4))
110 FORMAT(' ',////) CALL EXIT END 56

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